

Polymer Composites for Electronics Packaging Applications

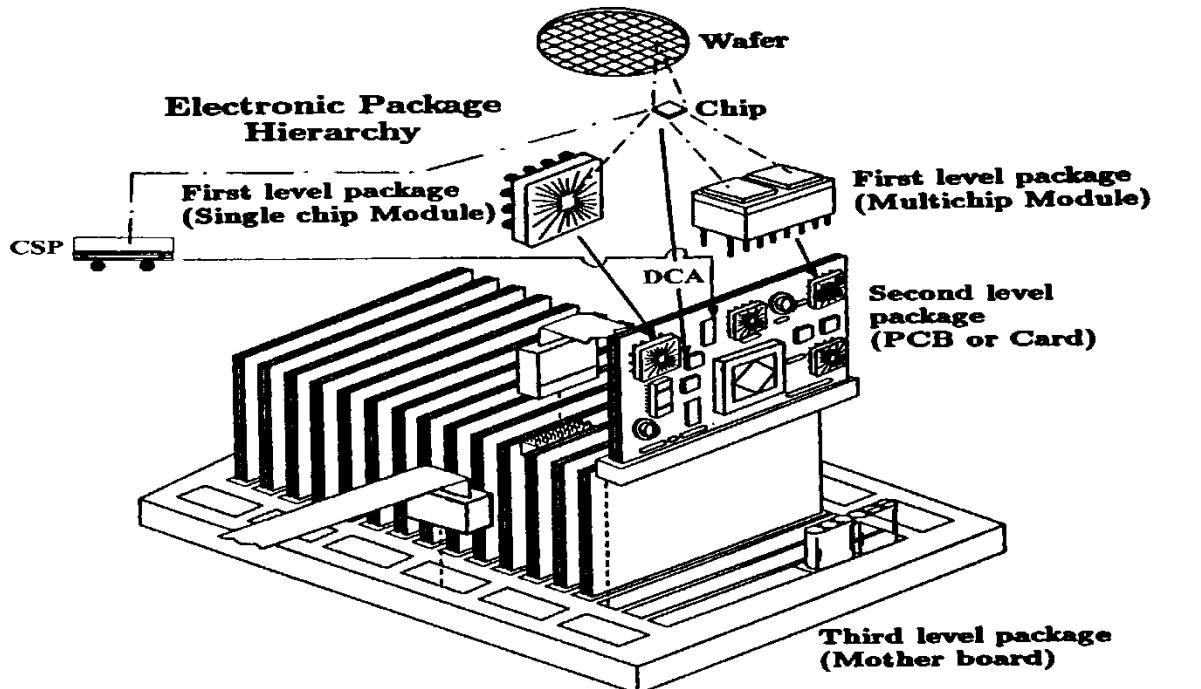
James E. Morris, Portland State University, Oregon USA

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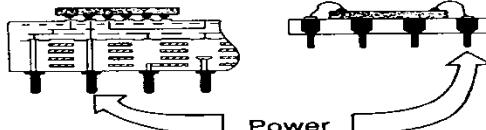


SIITME 2014 Bucharest

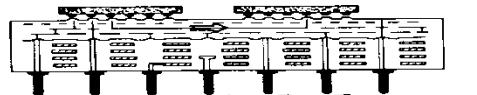
Supported in part by the IEEE CPMT Society Distinguished Lecturer program.



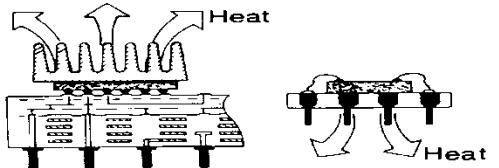
Power Distribution



Signal Distribution



Heat Dissipation



Package Protection

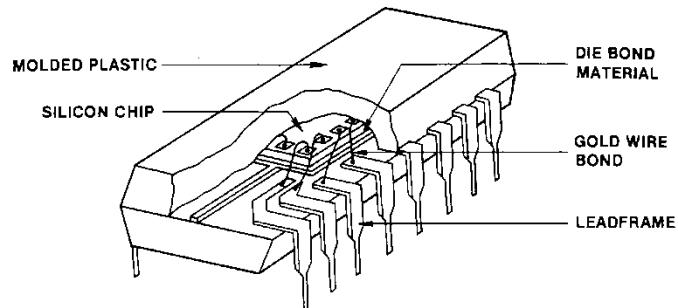
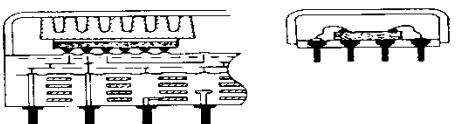


FIGURE 1-12. Cutaway view of a postmolded plastic package in the configuration of a dual-line package (DIP).

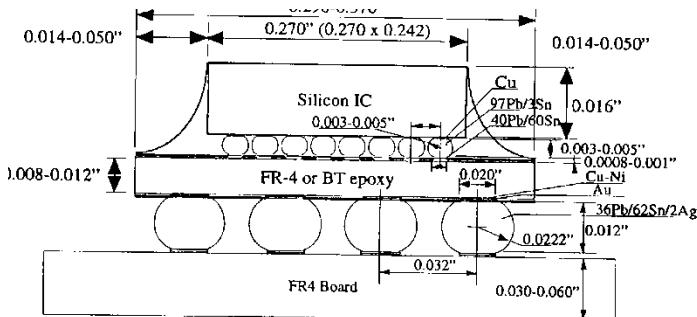


Figure 1: Schematic of a SLICC package.

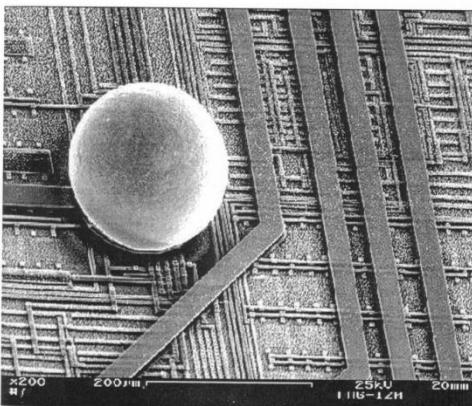


FIGURE 10.12. Comparison of typical WLP dimensions on a chip.

Packaging Issues

Thermal
3D Integration
Embedded Passives

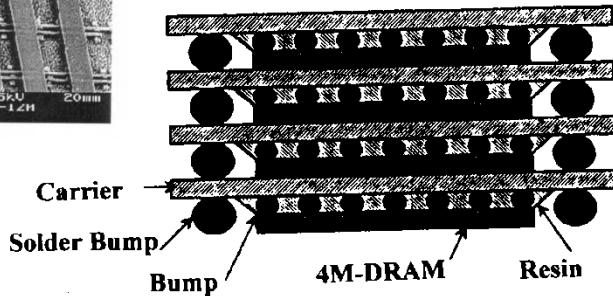
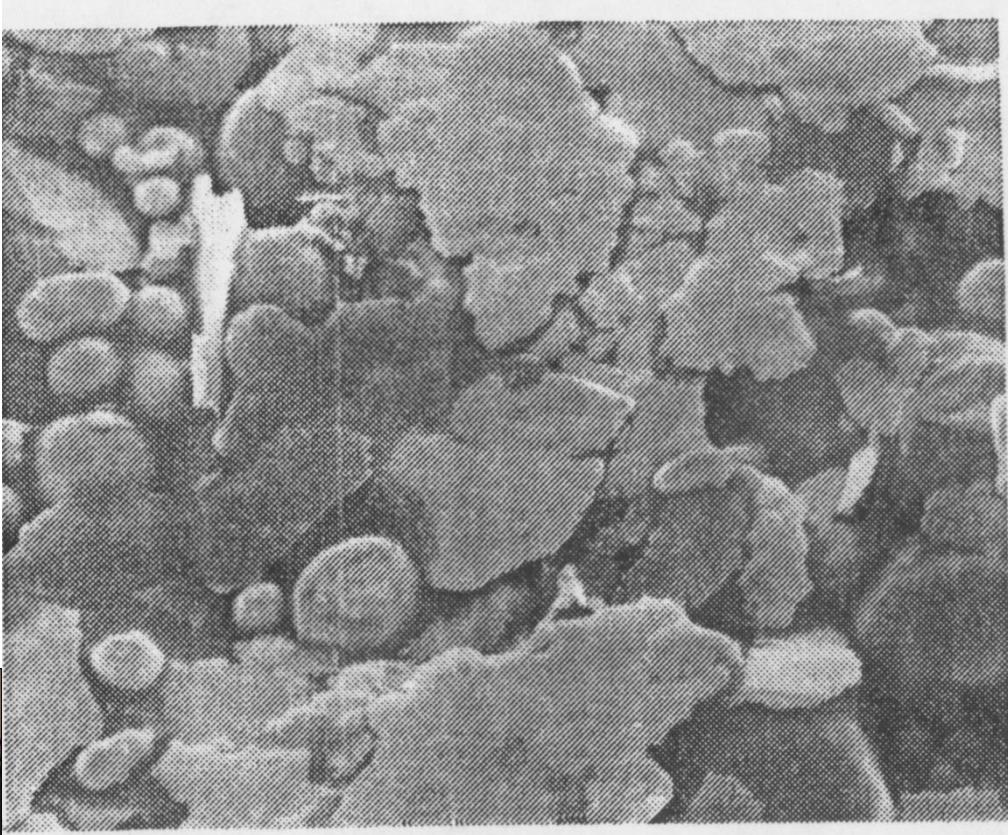
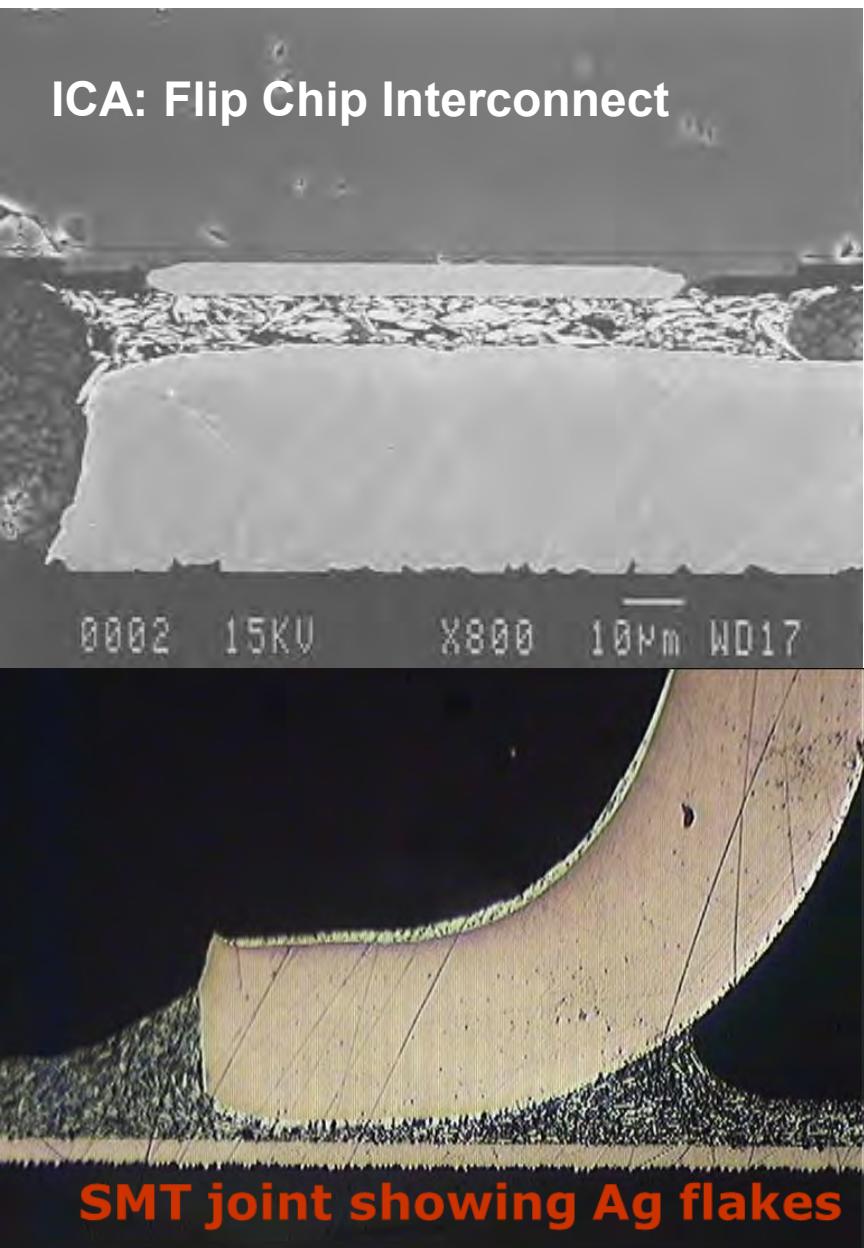


Figure 1.11. NEC's 3-D stack-up chip scale package (CSP) for memory devices.

- Polymer/metal composite example:
Isotropic Conductive Adhesive (ICA)
 - Percolation
 - Polymer cure
 - Electrical properties
 - Reliability:
 - Drop test
 - Galvanic corrosion
 - Miscellaneous
 - Magnetic alignment
 - Flip chip underfill filler
 - Nanoparticles
 - ICAs
 - Embedded components
 - Carbon nanotubes (CNTs) & graphene
 - Electrical & thermal

ICA: Isotropic Conductive Adhesives

ICA: Flip Chip Interconnect



Bi-modal distribution
e.g.
10µm diameter flakes (<1µm thick)
plus
1-3µm diameter powder (spheres)

Creep & Coffin-Manson Lifetimes: Comparisons with Solder (Rusanen)

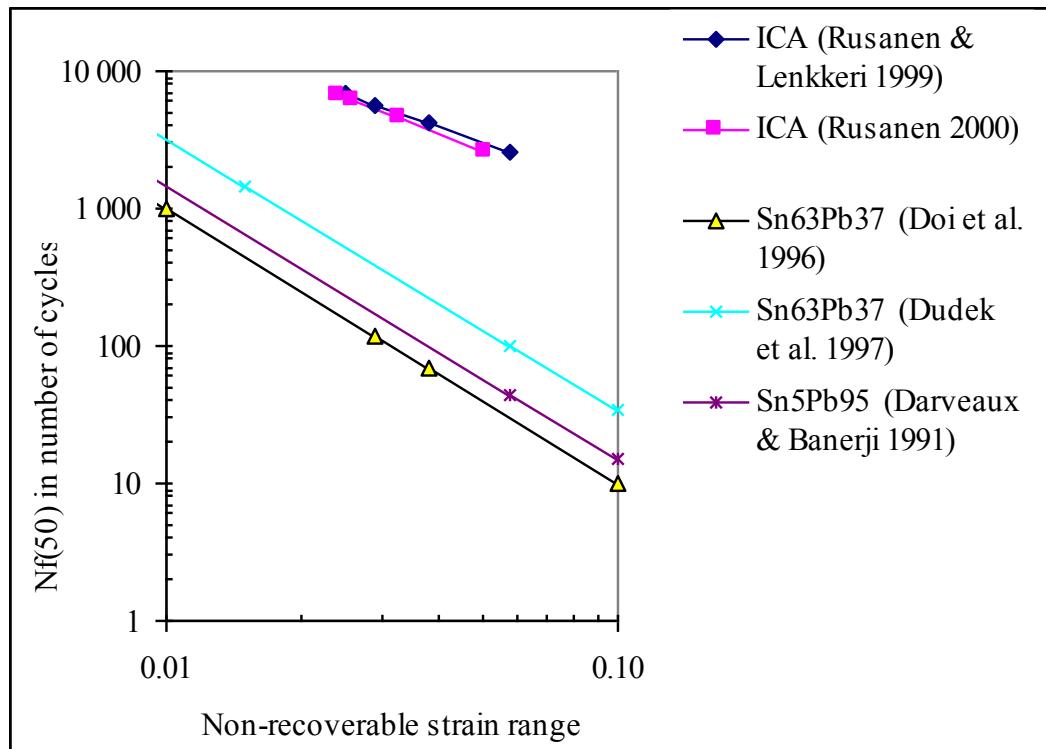
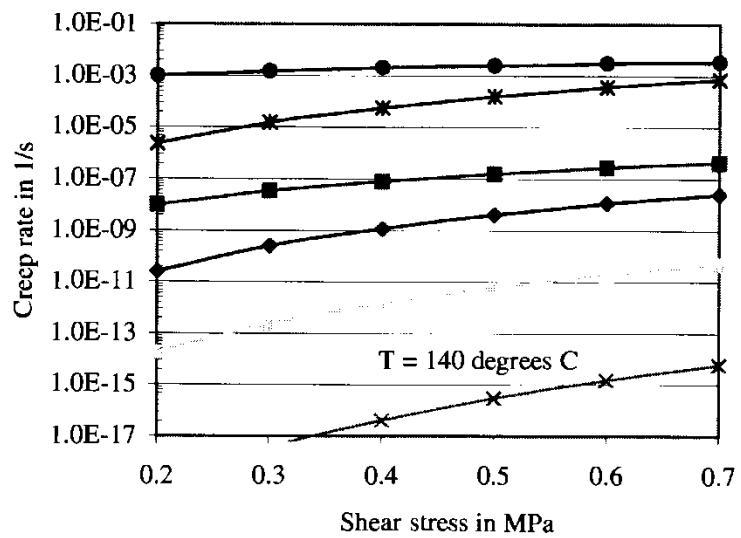
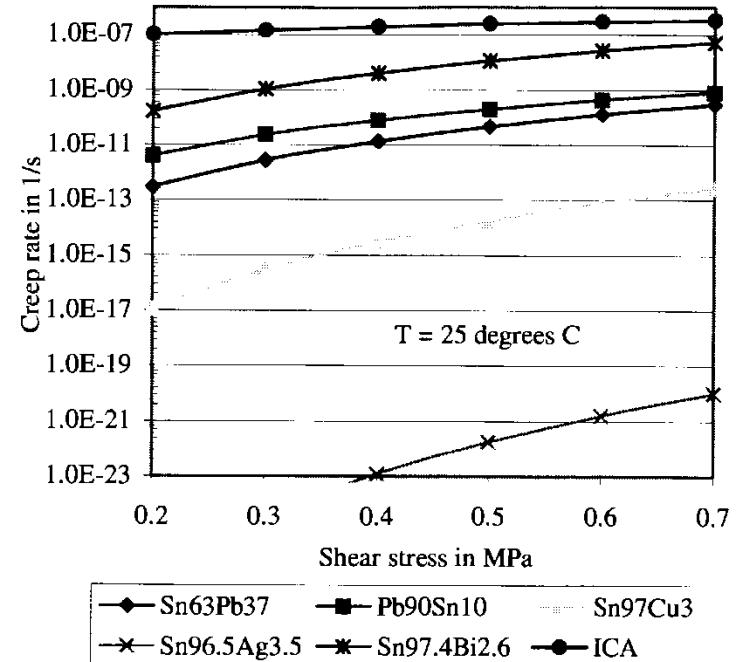
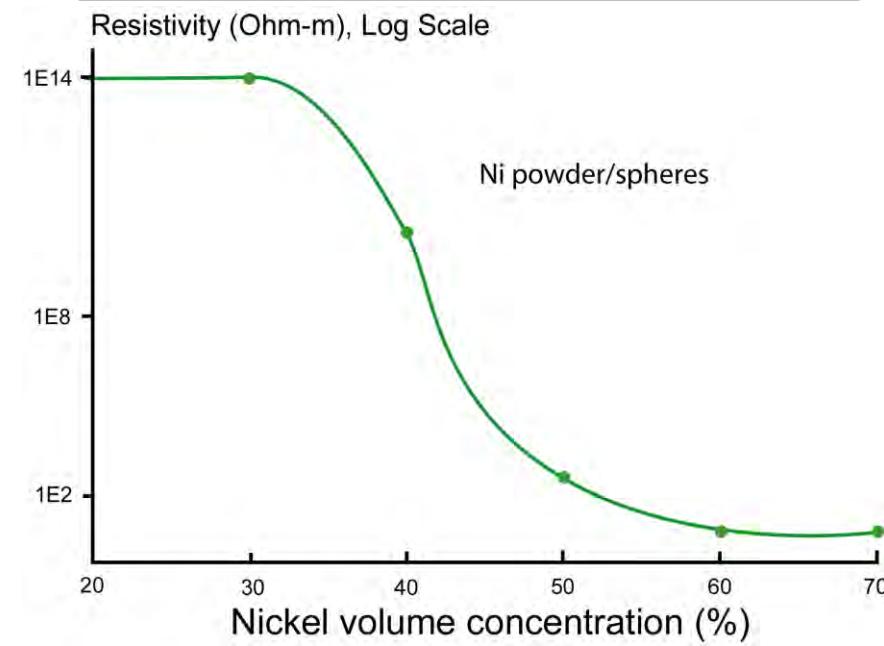
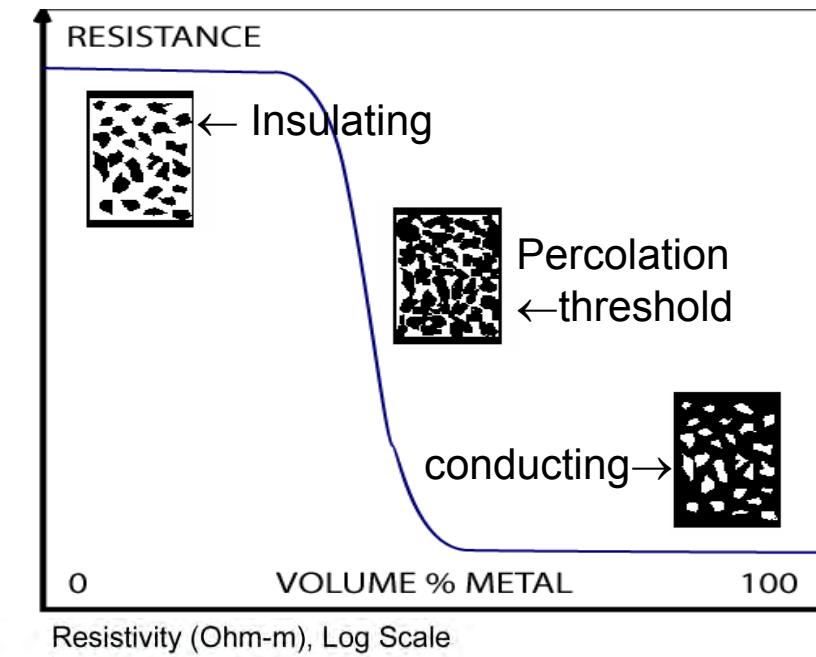
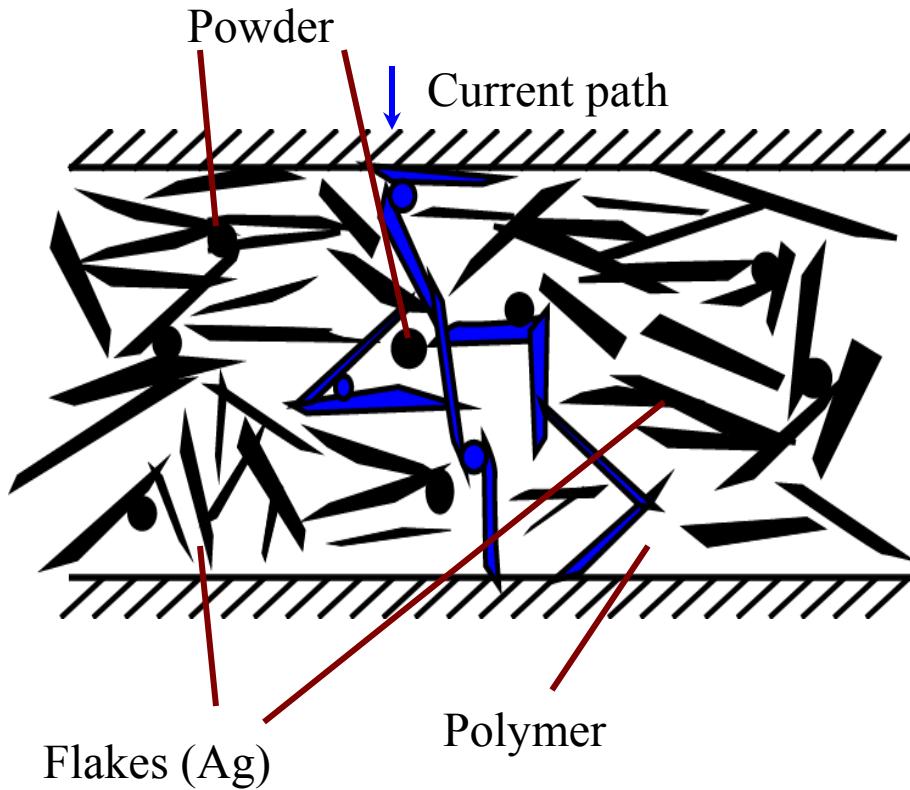


Figure 8. Creep rates of joining materials at temperatures of 25°C and 140°C.

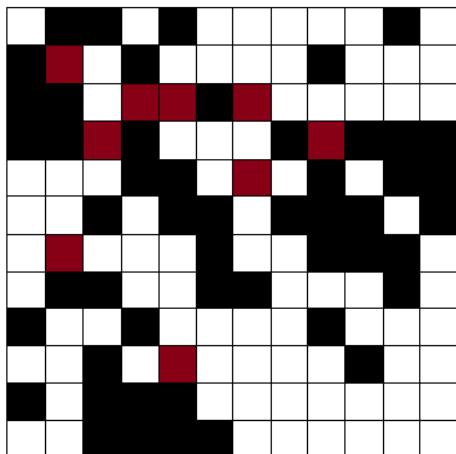
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ICA: Conducts by percolation

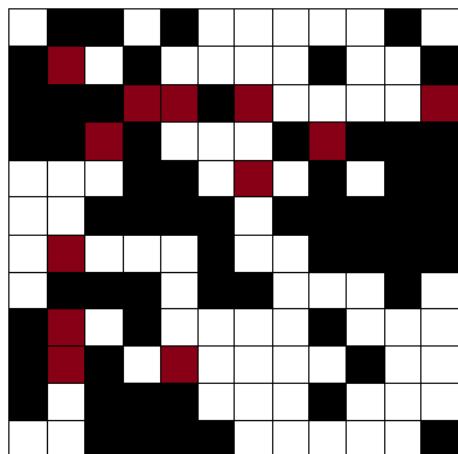


Site percolation modeling in a 12x12 array

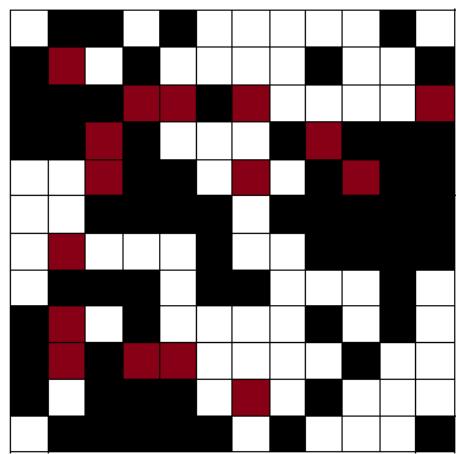
40%



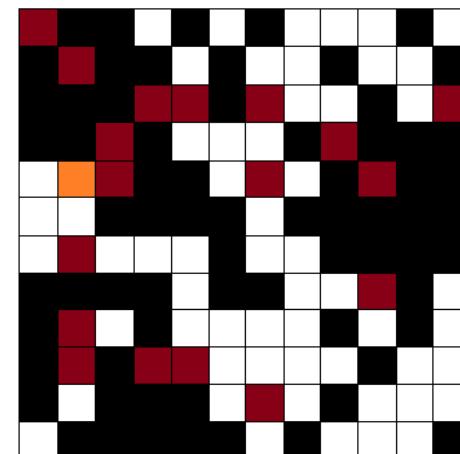
50%



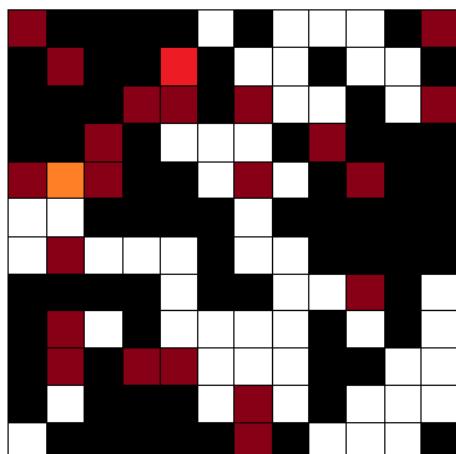
55%



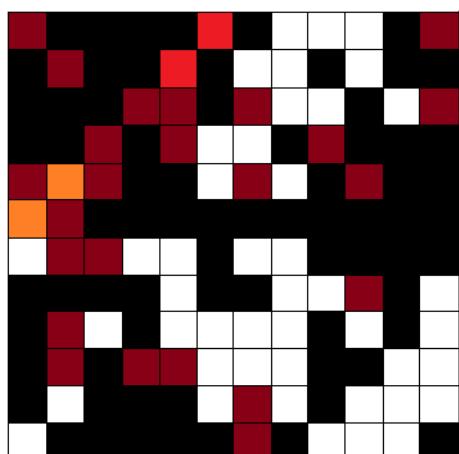
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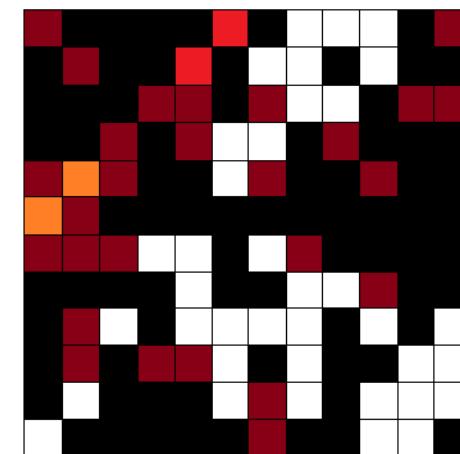
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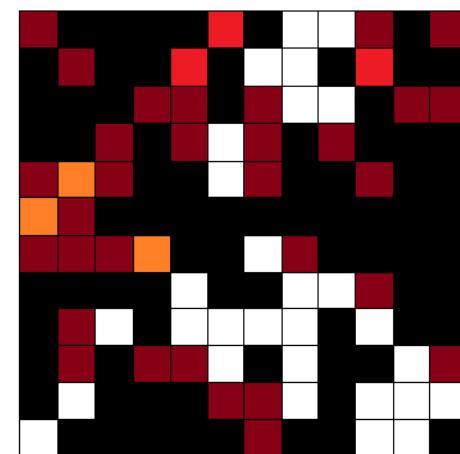
70%



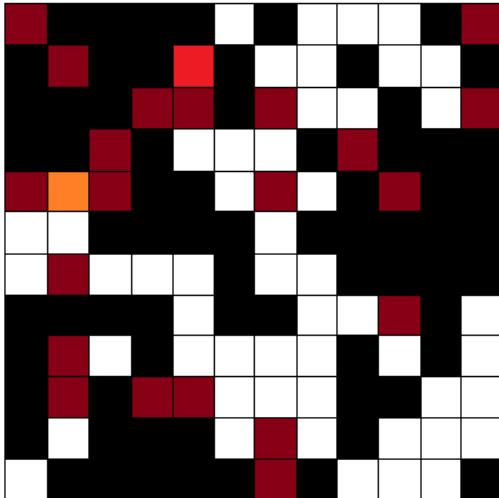
75%



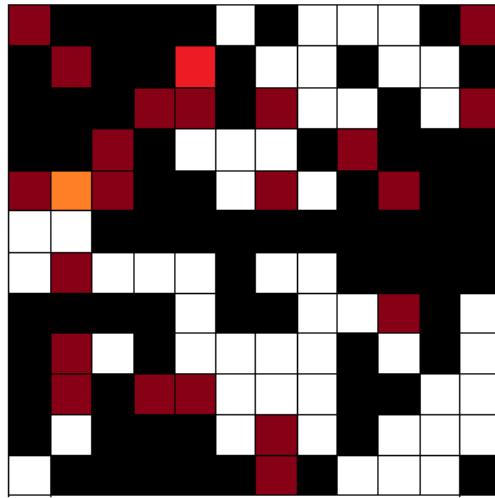
80%



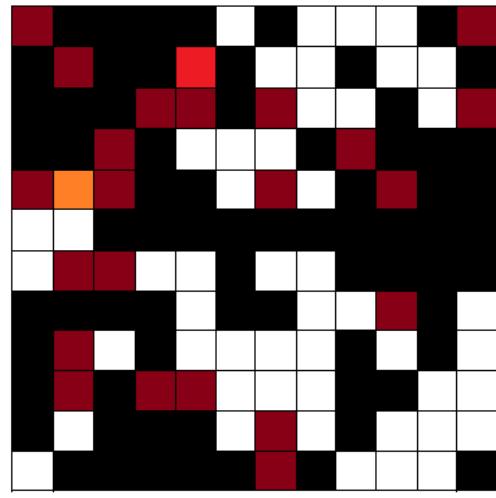
Critical percolation



65%



65%+1

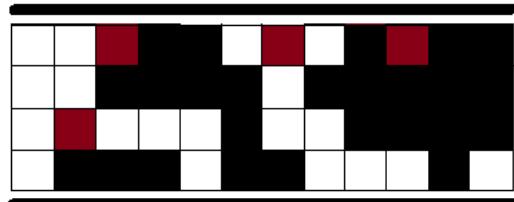


65%+2

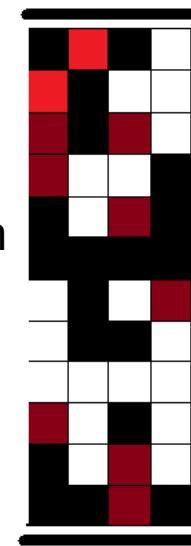
Percolating
Cluster (70%)



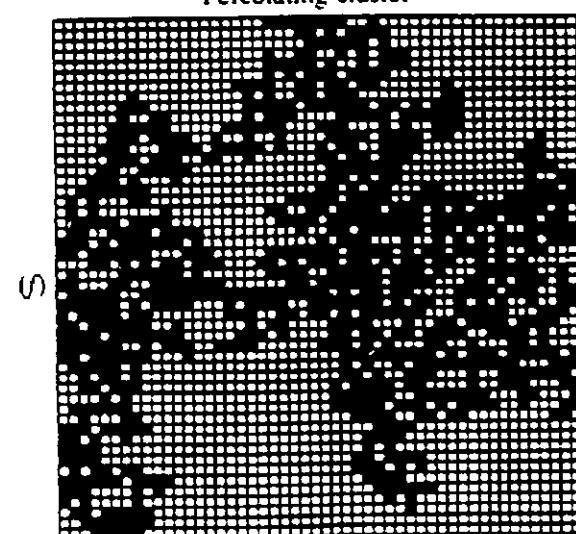
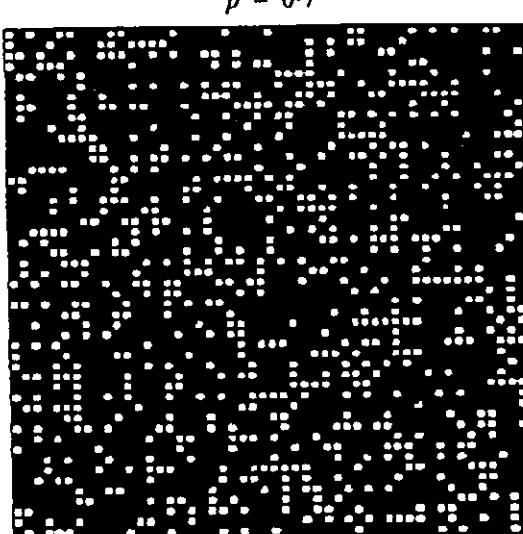
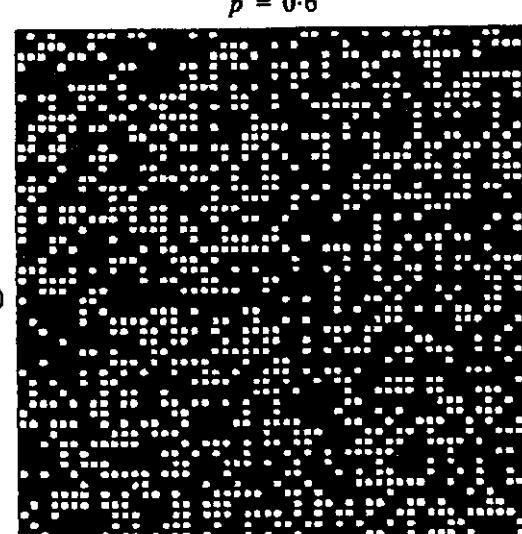
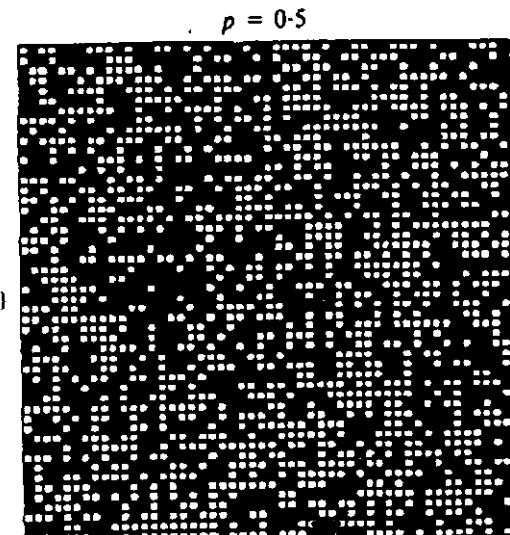
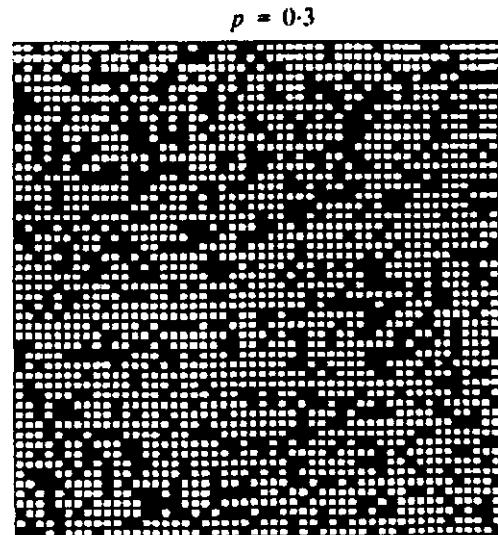
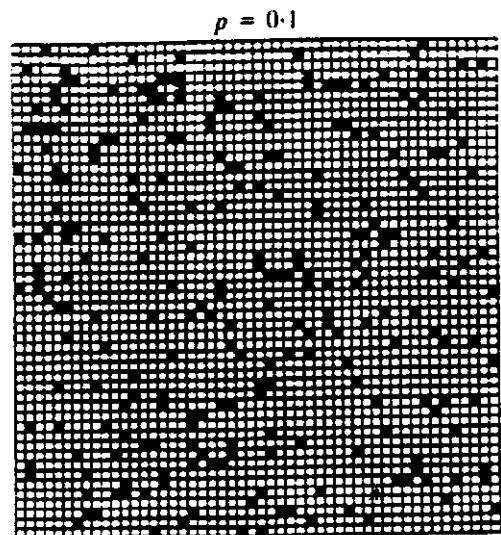
Size Effect
Middle 1/3 sections:
55%
conducts



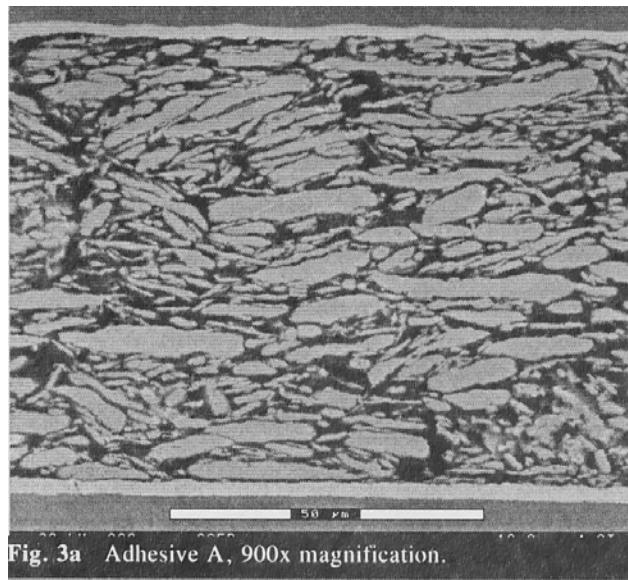
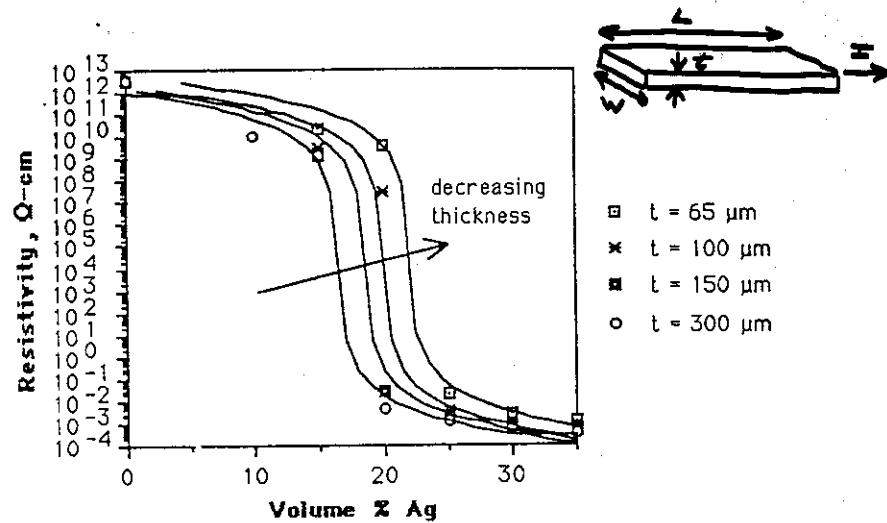
75%
no
conduction



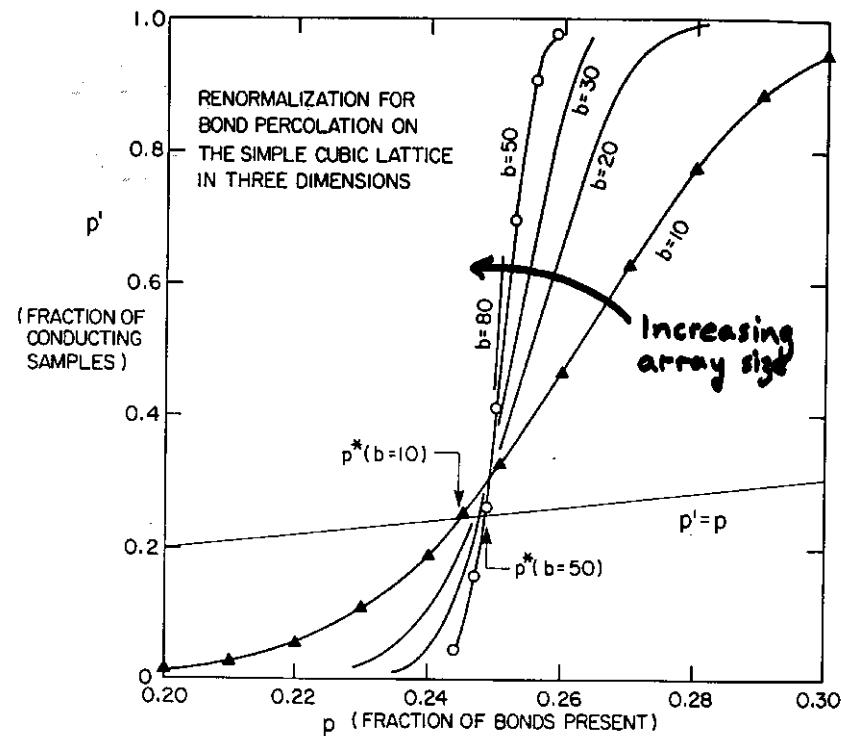
Monte Carlo Percolation Models



Percolation Threshold: Size Effects & Dispersion



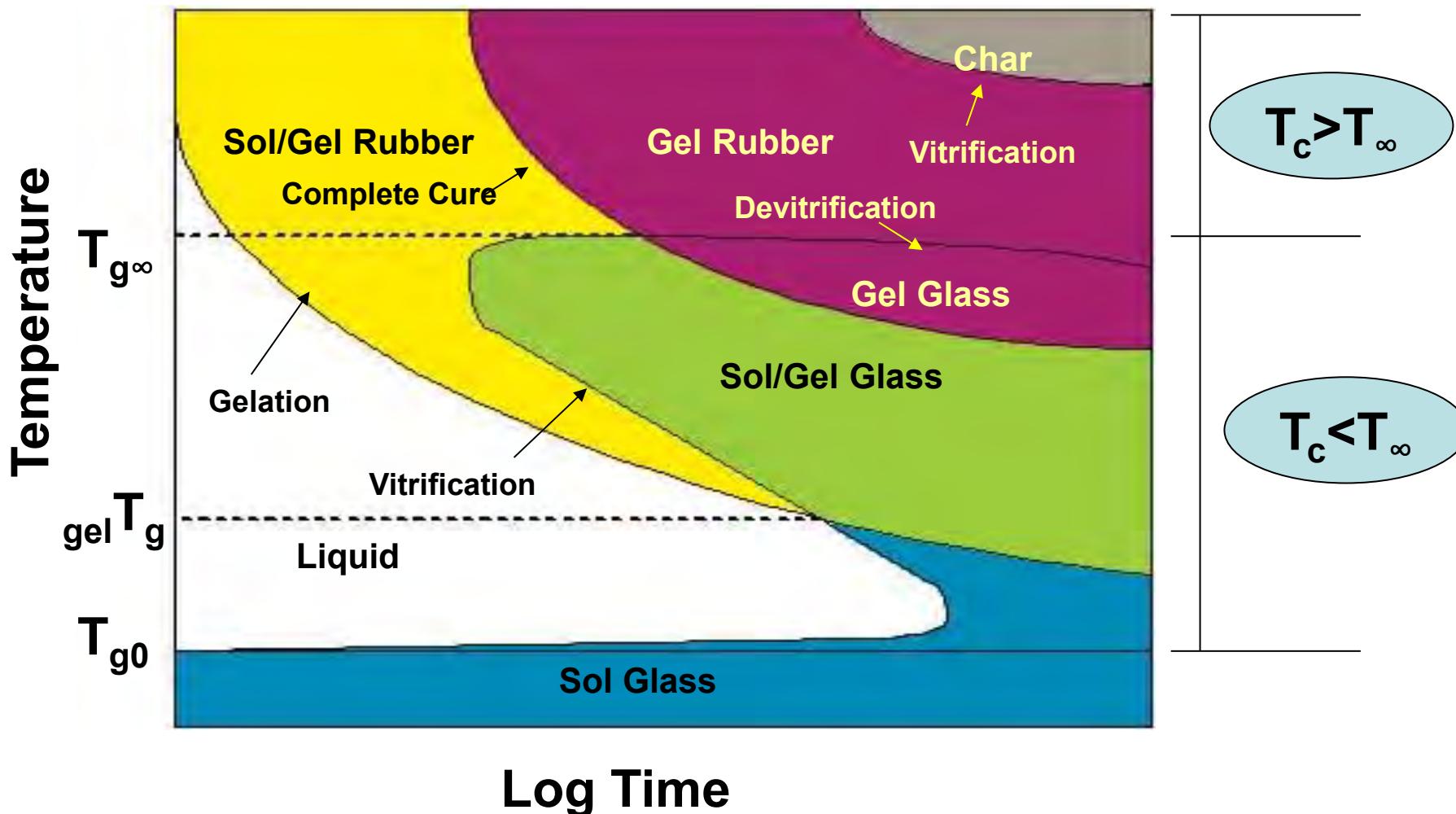
Constable et al
(Adhesives'98)



- Averaged simulations
- Reproducibility
 - small sizes
 - incr tolerances
 - higher Ag

- Polymer/metal composite example:
 Isotropic Conductive Adhesive (ICA)
- Percolation
- **Polymer cure**
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Polymer Cure Process



DSC: Differential Scanning Calorimetry

Directly determine degree of cure α & rate of cure $d\alpha/dt$

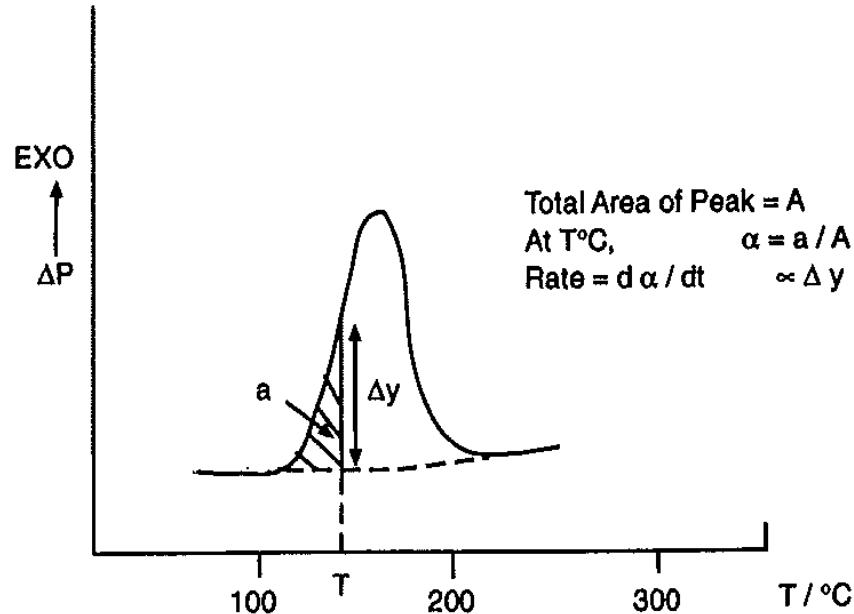
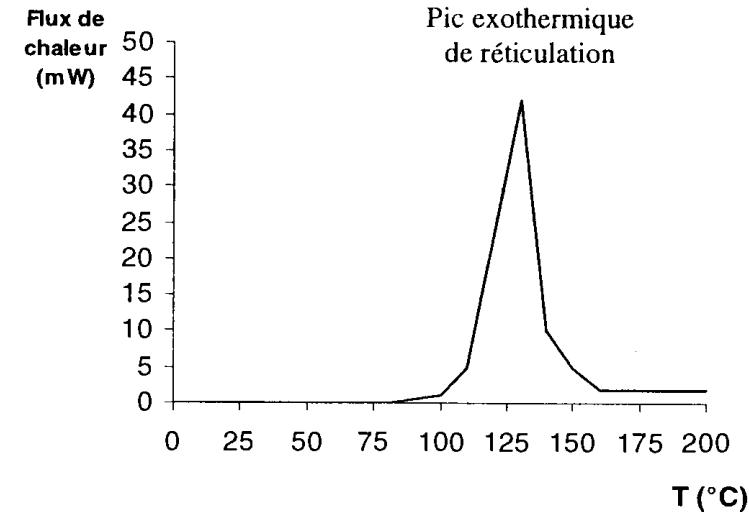
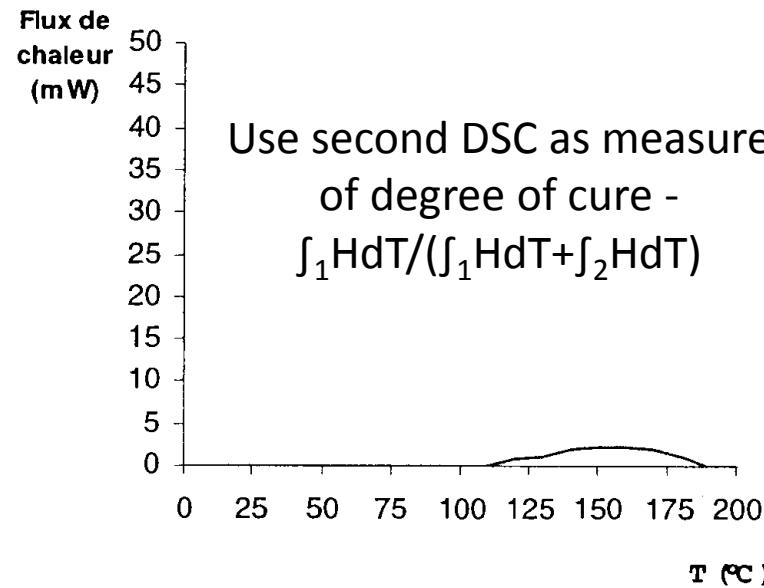


Figure 3.33 DSC curve for exothermic reaction showing measurement of partial and total areas.

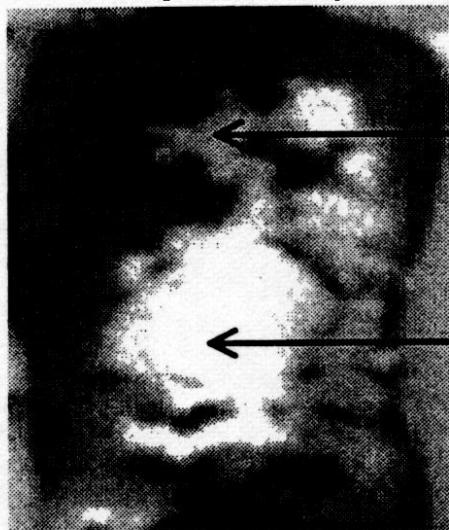


Use second DSC as measure of degree of cure -
 $\int_1 H dT / (\int_1 H dT + \int_2 H dT)$



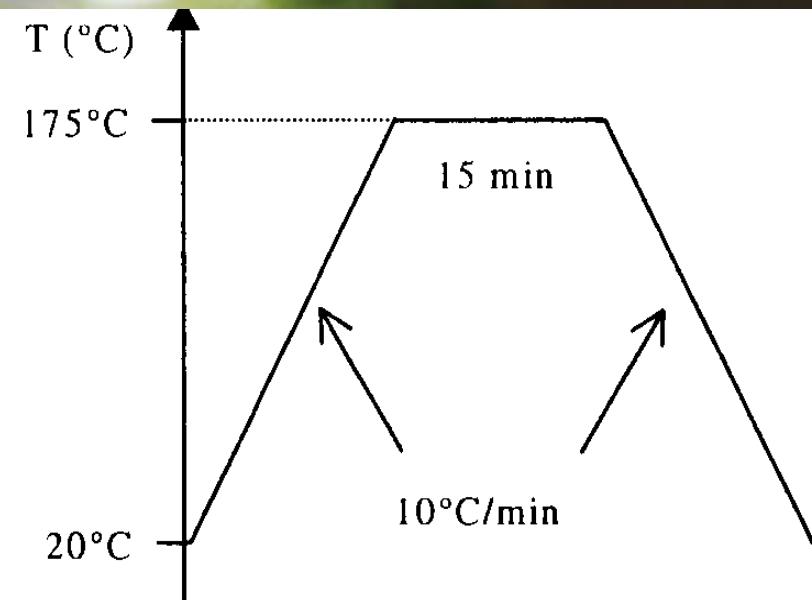
Delamination & Bubbles

Thermoplastic (Perichaud/Fremont)

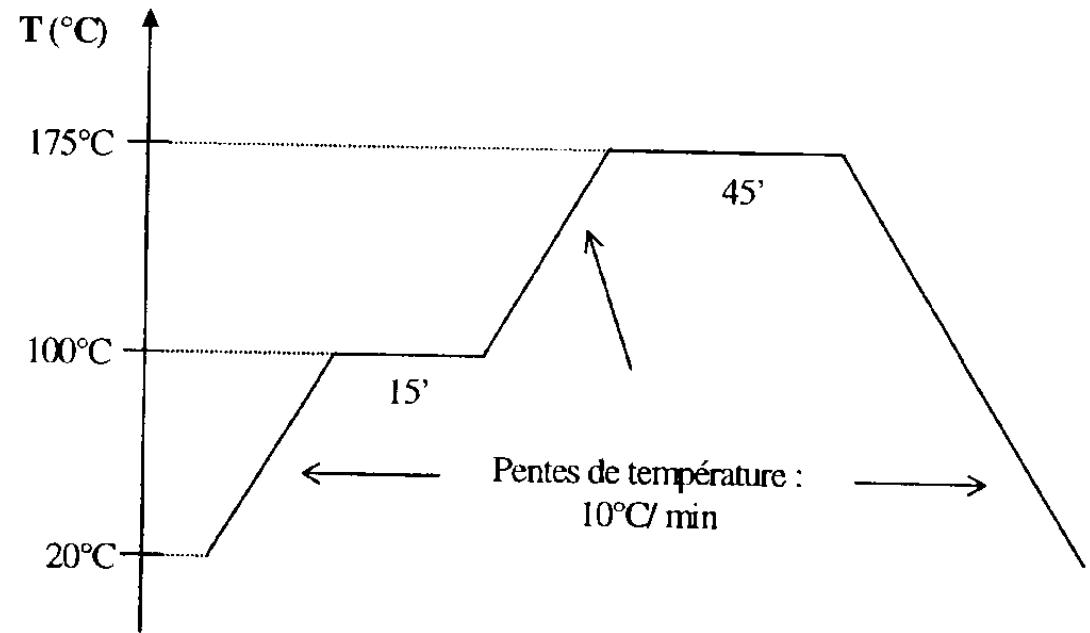
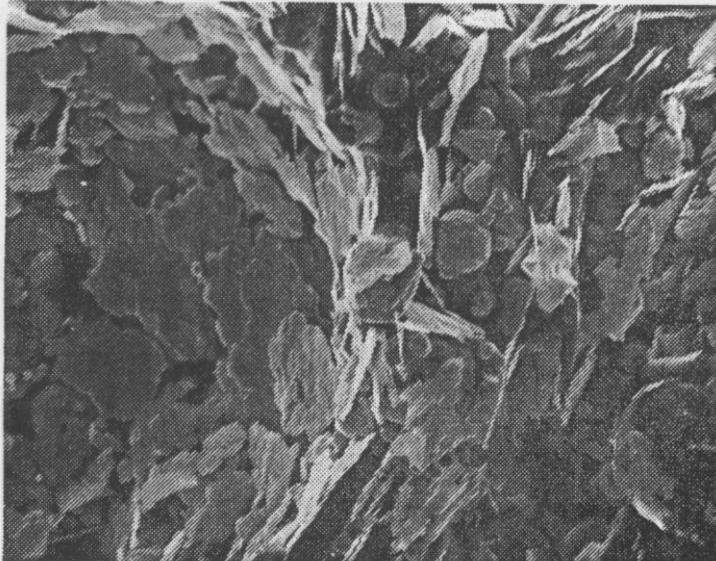


Délamination

Bulle



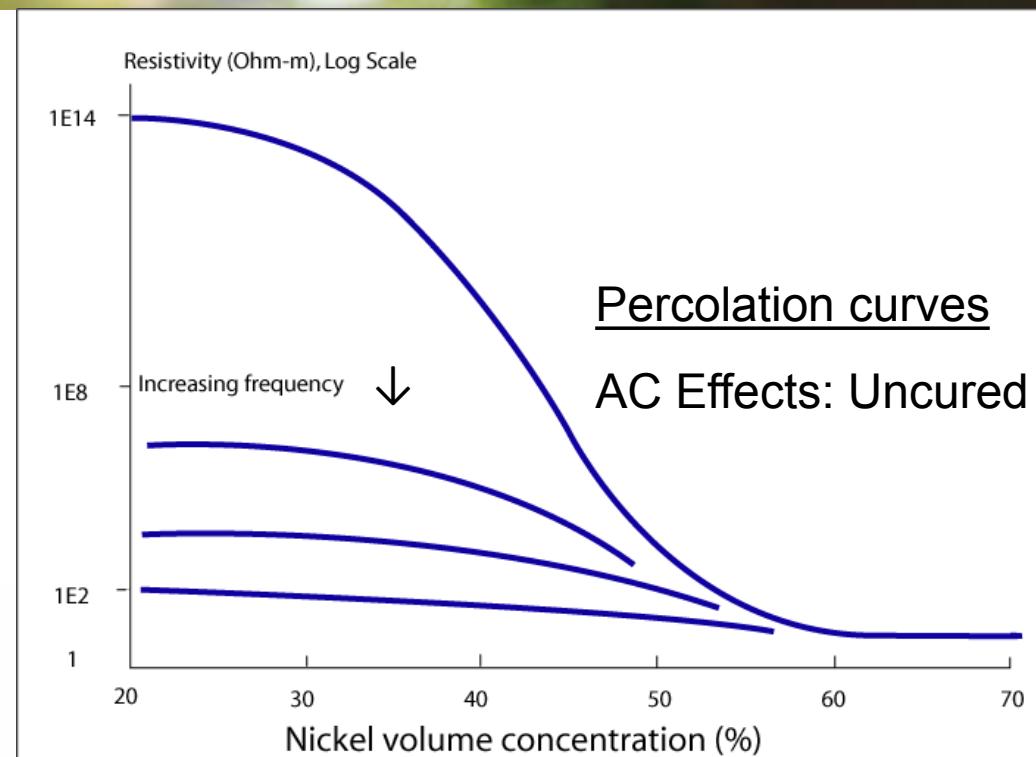
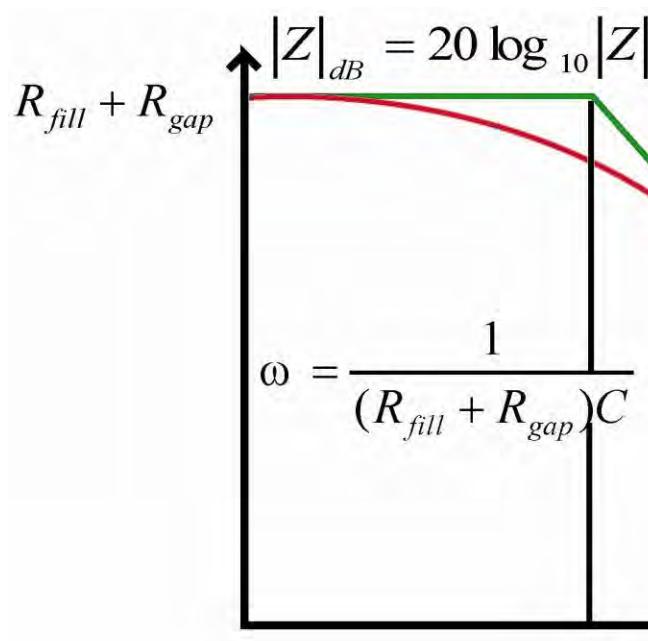
Thermoset (Morris/Li)



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Frequency Effects:

Tunnel Gaps?

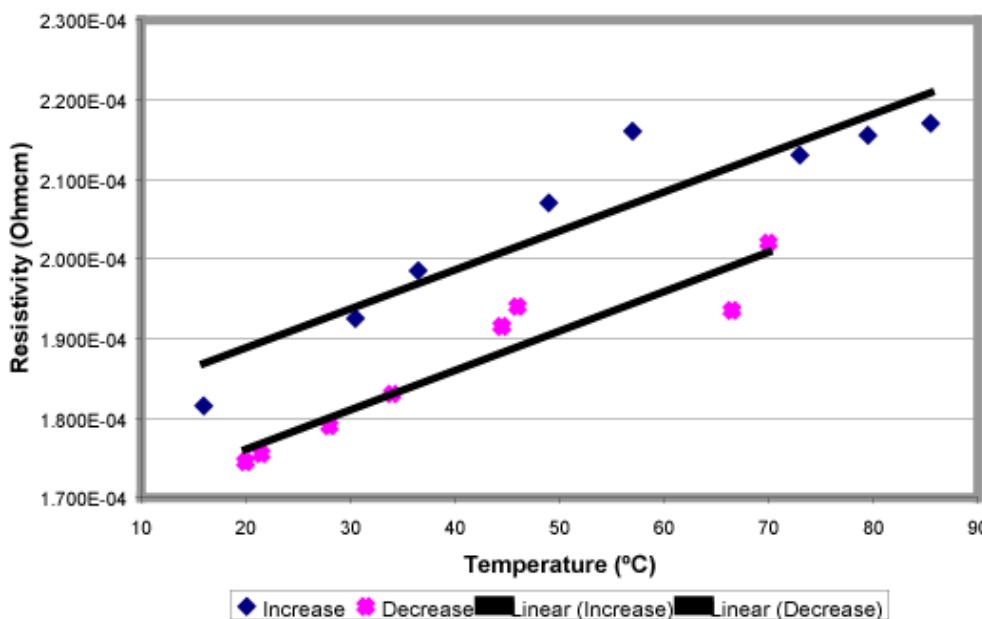
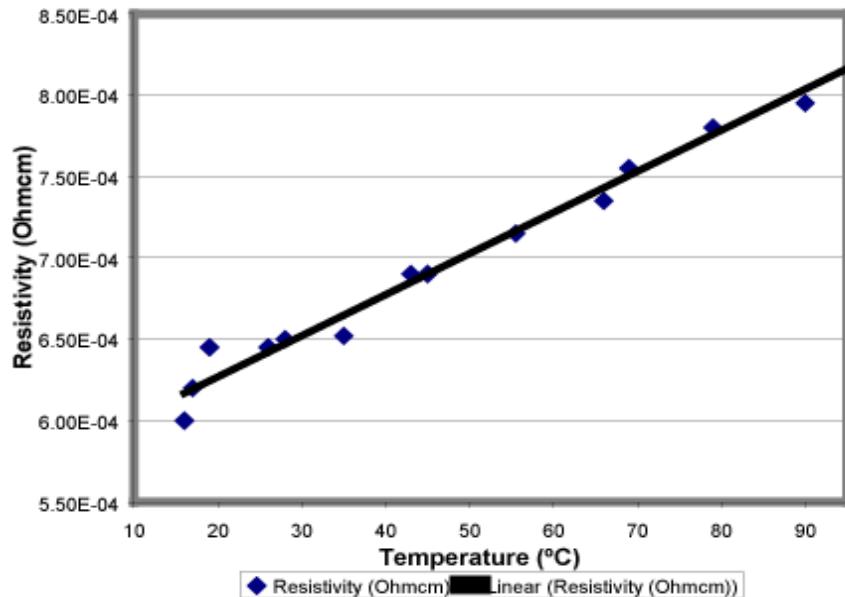


$$\omega = \frac{1}{R_{fill}C}$$

R_{fill}

$\log_{10} \omega$

Experimental: TCR Results



$$TCR_{ICA} \approx TCR_{Ag}$$

$$\therefore R_{ICA} \approx R_{Ag}$$

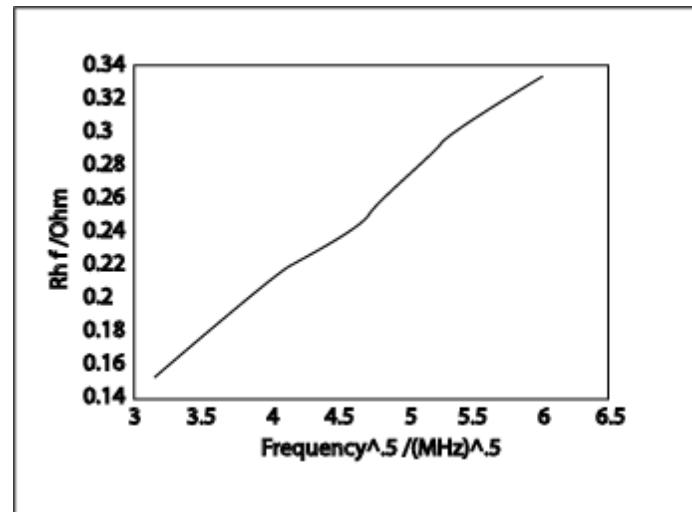
Contact R negligible

Resistivities for various temperatures.

- Brass stenciled CT-5047-02 thermoset sample (TCR=0.0039/°C).**
- (b) CSM-933-65-1 screen printed thermoplastic sample {TCR=0.0038/°C}**

Frequency Effects: Skin Effect

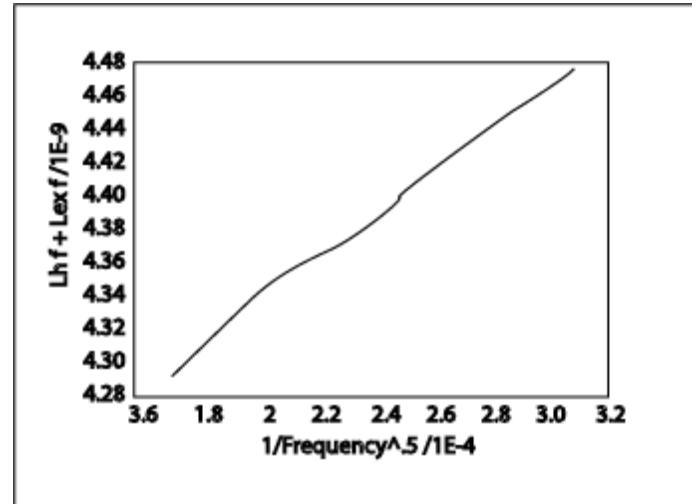
R



$$\sqrt{f}$$

This graph shows the linear relationship between the resistance at high frequencies and the square root of frequency

L



$$1/\sqrt{f}$$

This figure exhibits the linear relationship of the inductance at high frequencies with $f^{.5}$

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Impact Strength/Drop Test (Tong)

Adhesion tests passed

Devices fall off PWB if dropped

Large devices fail; small OK

No correlation between drop test results and adhesion strength testing

**Complex shear modulus
Storage and loss moduli**

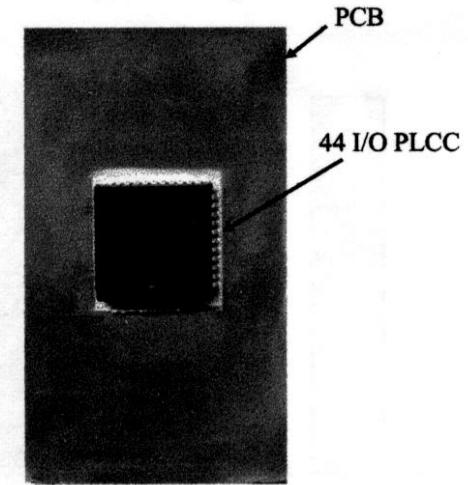


Figure 2. A Photograph of a Drop Test Sample

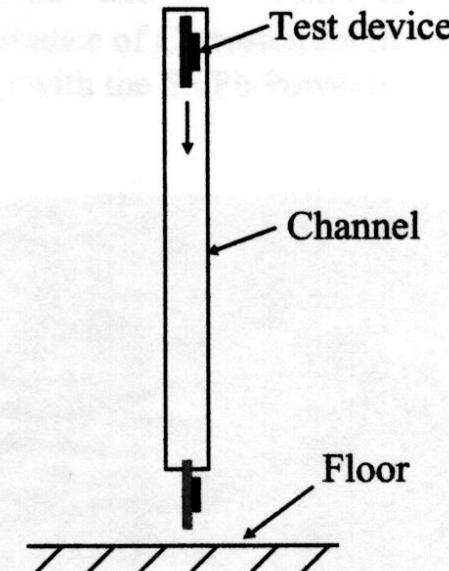
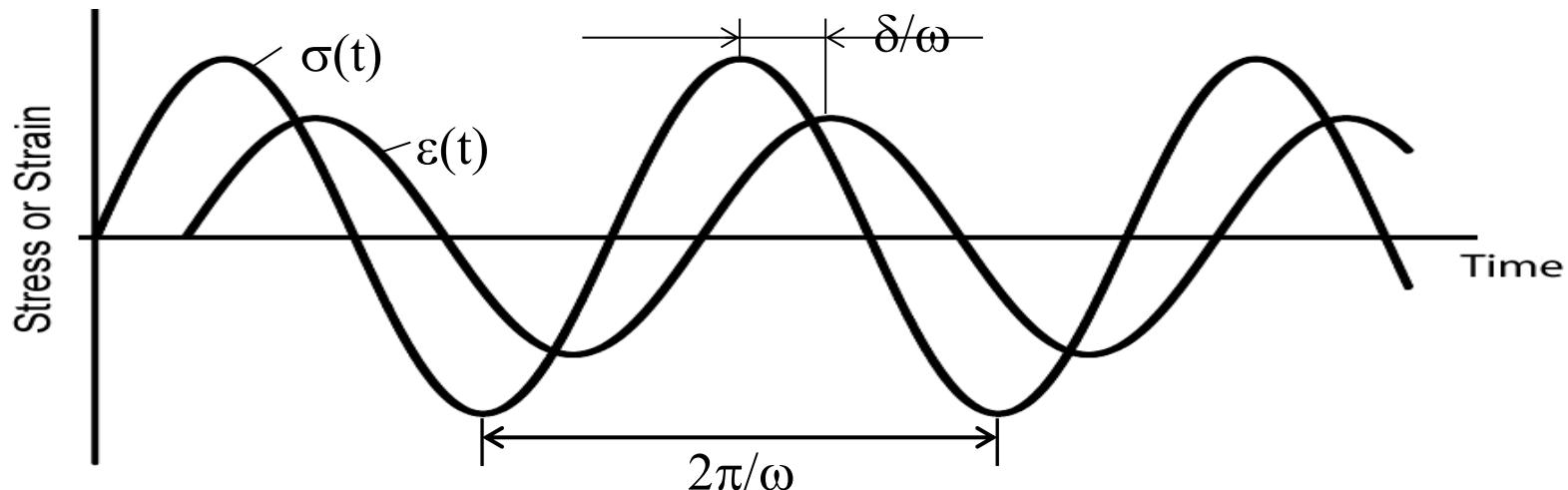


Figure 3. A Schematic of Drop Test Set-up

Shear Stress σ & Strain ϵ Complex Shear Modulus



Shear stress $\sigma = S/A$

Shear strain $\epsilon = a/h$

$$\sigma = G\epsilon$$

Elastic shear modulus

$$G = G' + iG''$$

Loss tangents:

$$\tan \delta = G''/G'$$

Charge density $\sigma = Q/A$

Electric field $E = V/d$

$$\sigma = \epsilon E \quad [Q = (\epsilon A/d)V]$$

Dielectric constant

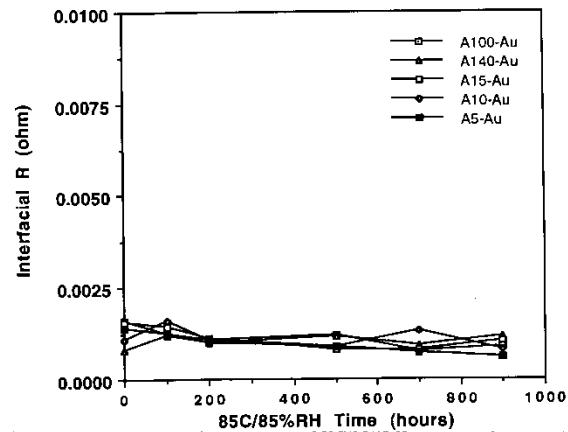
$$\epsilon = \epsilon' + i\epsilon''$$

$$\tan \delta = \epsilon''/\epsilon'$$

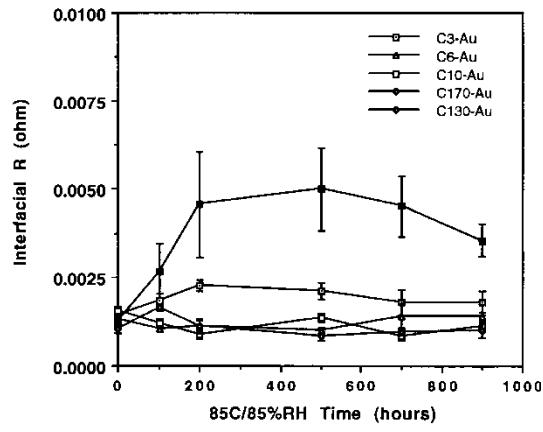
- **High $\tan \delta$ by $T_{amb} > T_g \rightarrow$ high CTE**

Contact R 85/85: Au & Cu contacts

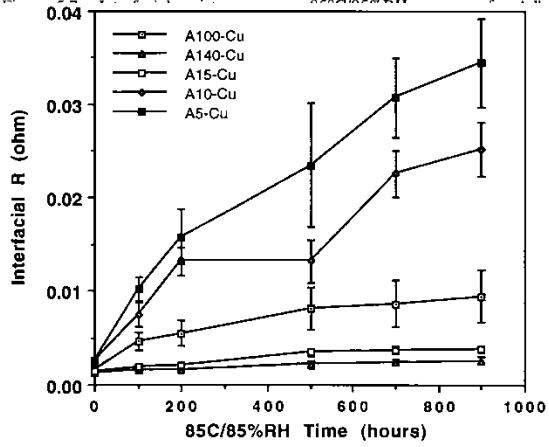
A on Au



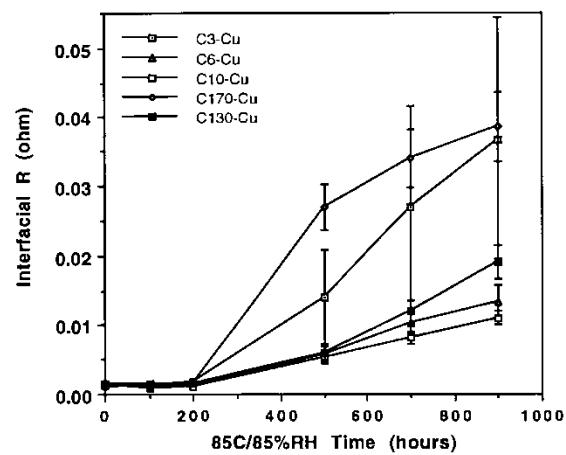
C on Au



A on Cu



C on Cu



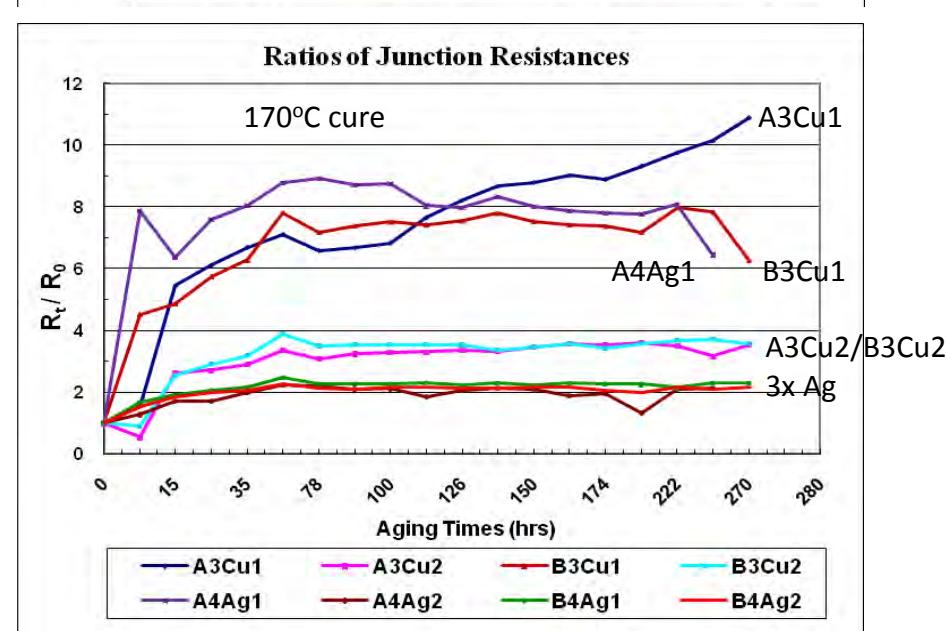
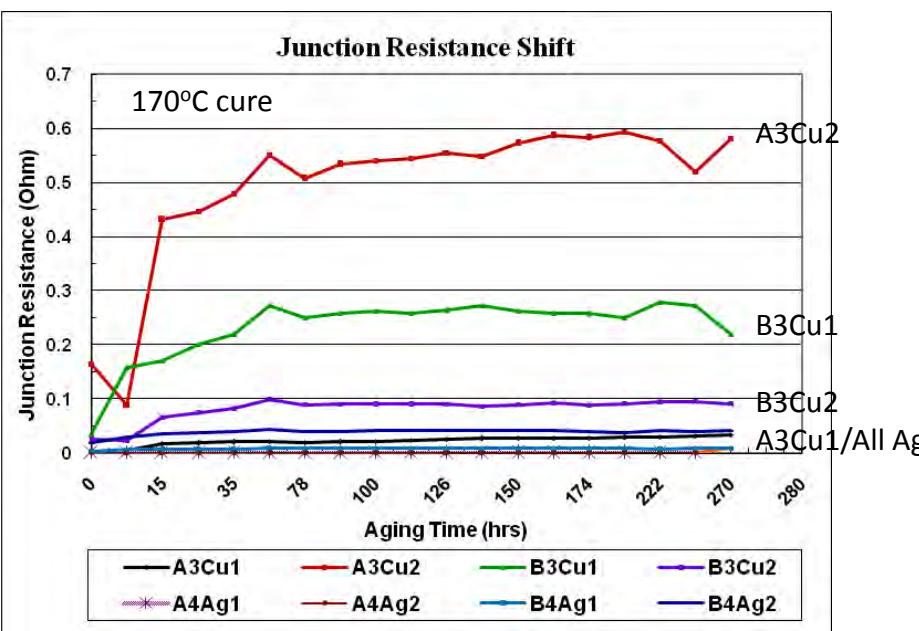
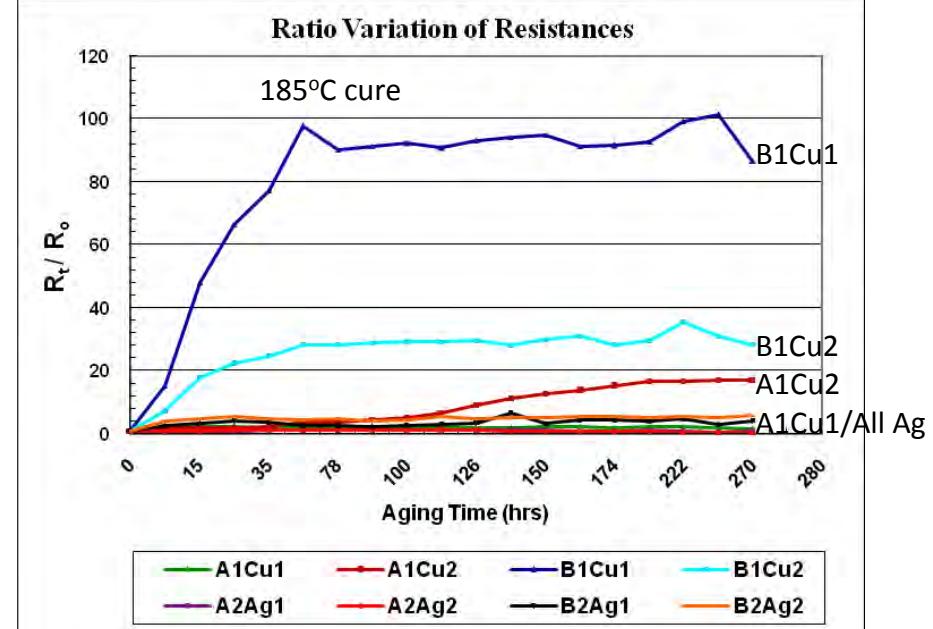
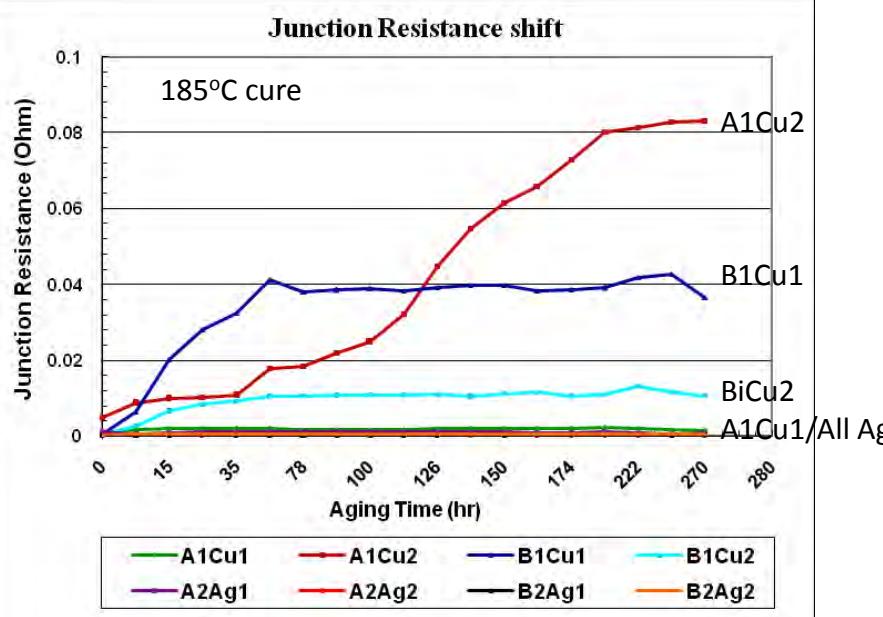
(Li & Morris)

Galvanic Corrosion

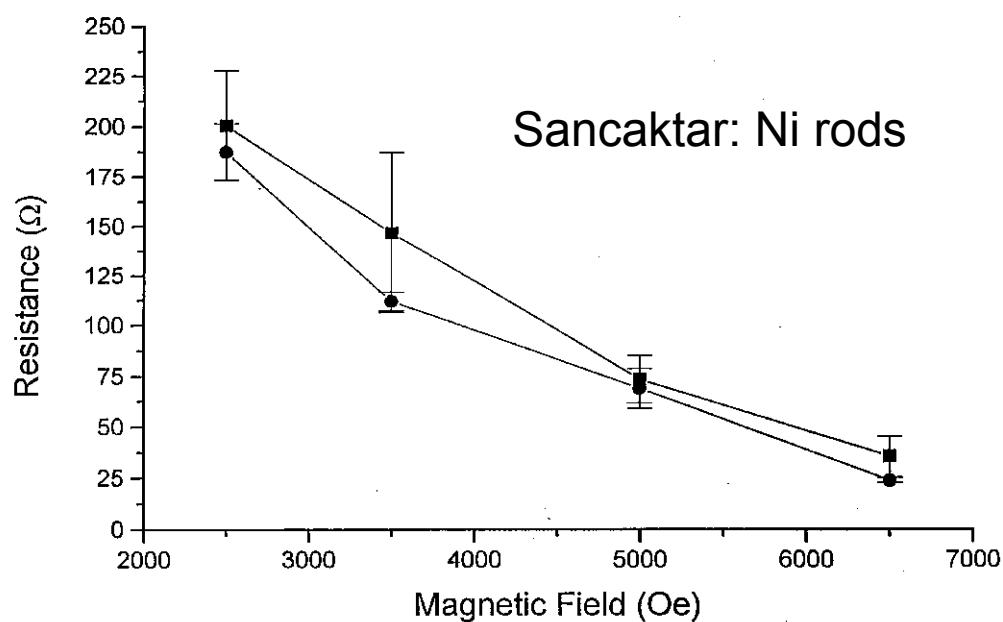
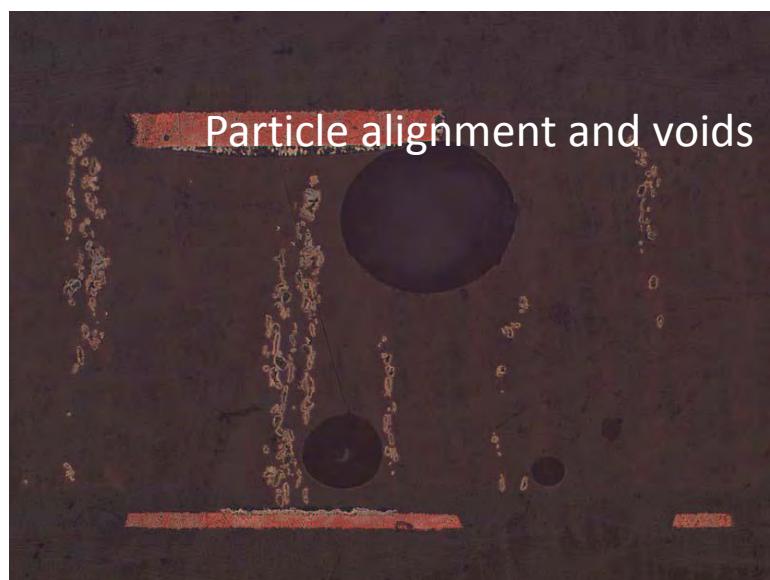
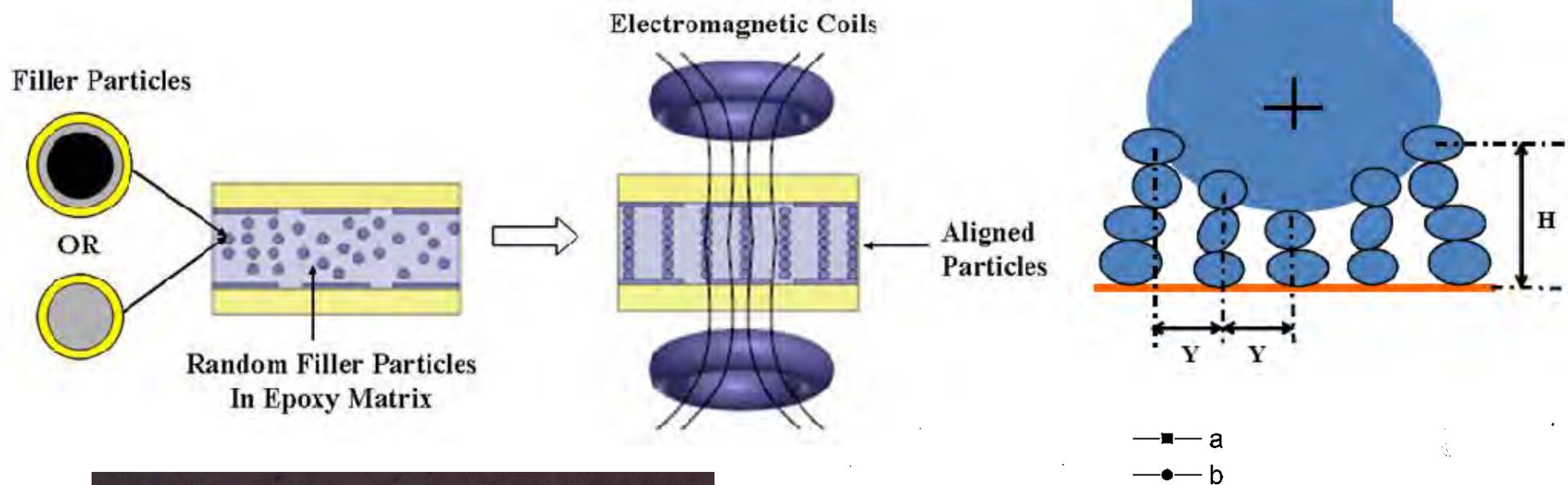
Electrode Reaction	Normal Potential
$\text{Au} - 3\text{e}^- = \text{Au}^{3+}$	1.50 v
$\text{Pt} - 2\text{e}^- = \text{Pt}^{2+}$	1.20 v
$\text{Ag} - \text{e}^- = \text{Ag}^+$	0.80 v
$\text{Cu} - \text{e}^- = \text{Cu}^+$	0.52 v
$\text{H}_2\text{O} + \text{O}_2 + 4\text{e}^- = 4\text{OH}^-$	0.40 v
$\text{Cu} - 2\text{e}^- = \text{Cu}^{2+}$	0.34 v
$\text{Pb} - 2\text{e}^- = \text{Pb}^{2+}$	- 0.13 v
$\text{Sn} - 2\text{e}^- = \text{Sn}^{2+}$	- 0.14 v
$\text{Ni} - 2\text{e}^- = \text{Ni}^{2+}$	- 0.25 v

ICA: Lee, Cho, & Morris, Proc. EMAP 2007

Ag-ICA performance comparison on Cu and immersion-Ag PWB contacts



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Nano-Silica Flip-Chip Underfill

Compare CTE mis-match:

$$\text{Si} = 4\text{-}5 \text{ ppm}/^\circ\text{C}$$

$$\text{Ag} = 20 \text{ ppm}/^\circ\text{C}$$

$$\text{Epoxy} = 54 \text{ ppm}/^\circ\text{C}$$

$$\text{FR4} = 36 \text{ ppm}/^\circ\text{C}$$

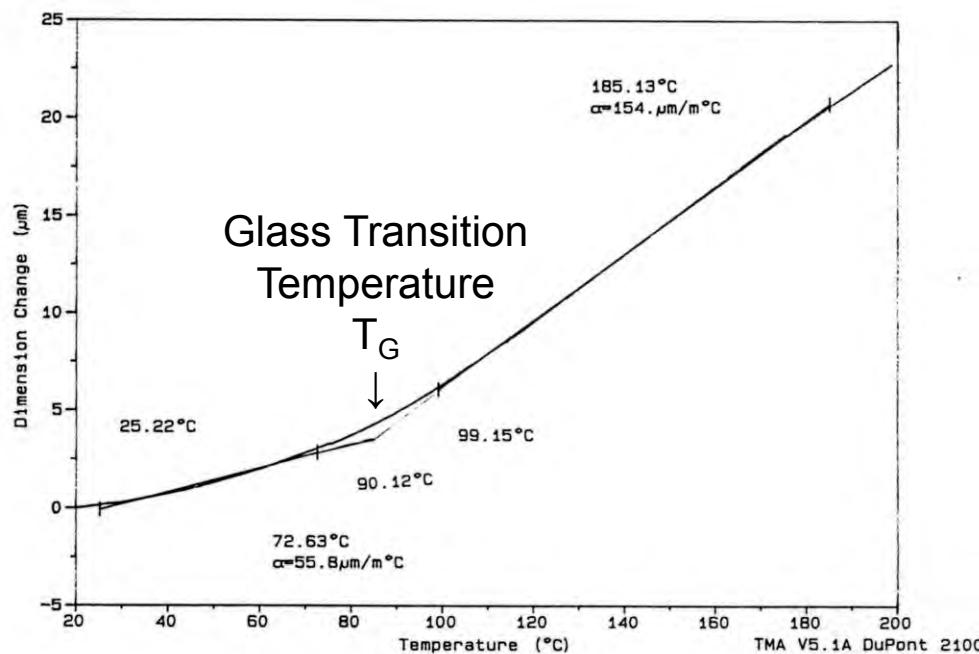


Figure 4.4: Typical TMA graphs for Adhesive A showing CTE above and below T_g .

Table 4.3. TMA experimental results for cured block samples.

Materials	T_g ($^\circ\text{C}$)	CTE ($< T_g$) ($\mu\text{m}/\text{m}^\circ\text{C}$)	CTE ($> T_g$) ($\mu\text{m}/\text{m}^\circ\text{C}$)
Adhesive A	90	56	155
Adhesive B	90	61	168
Adhesive C	90	78	218

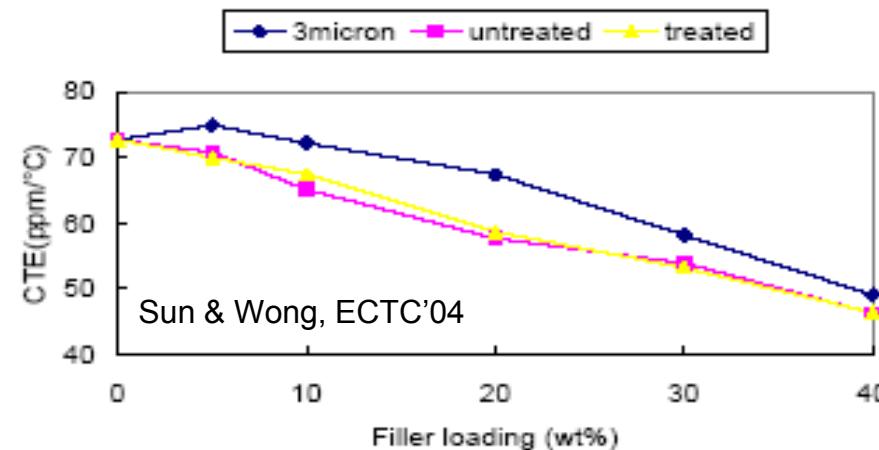
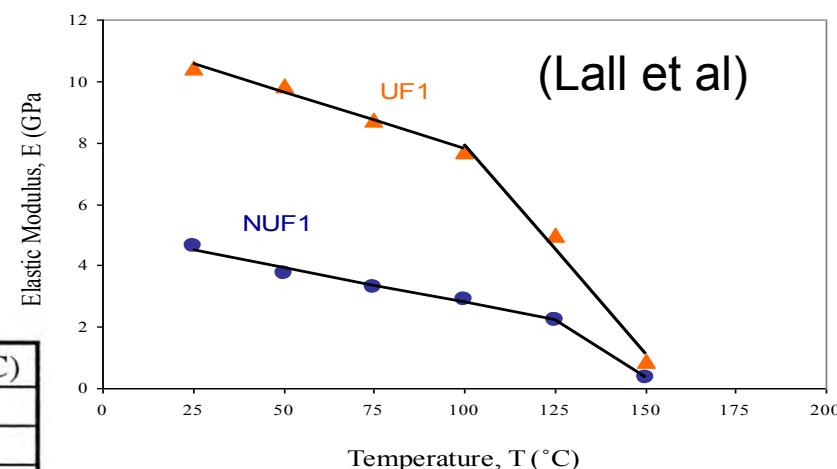


Figure 6 CTE of silica filled composite underfills

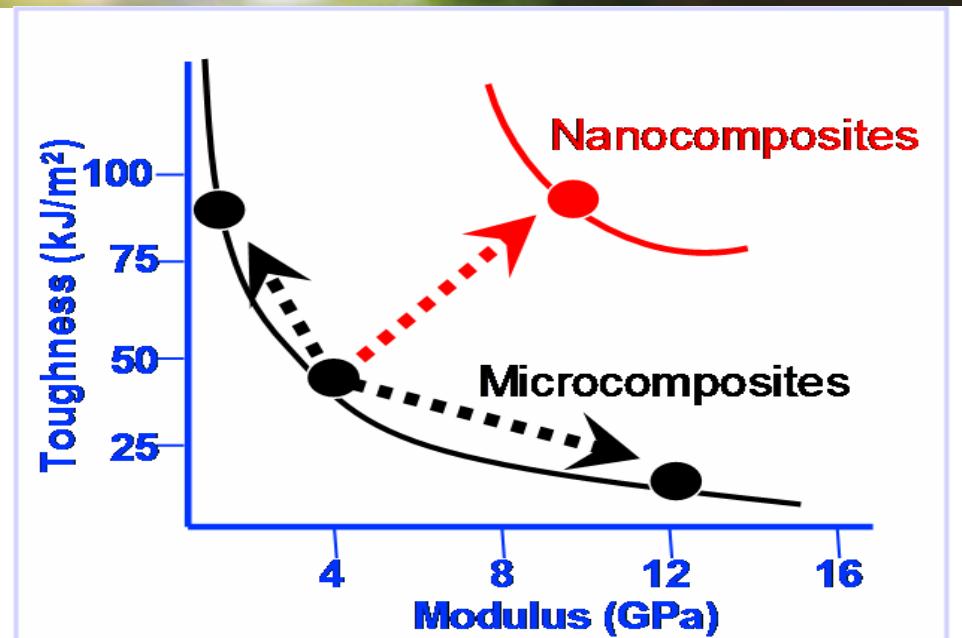
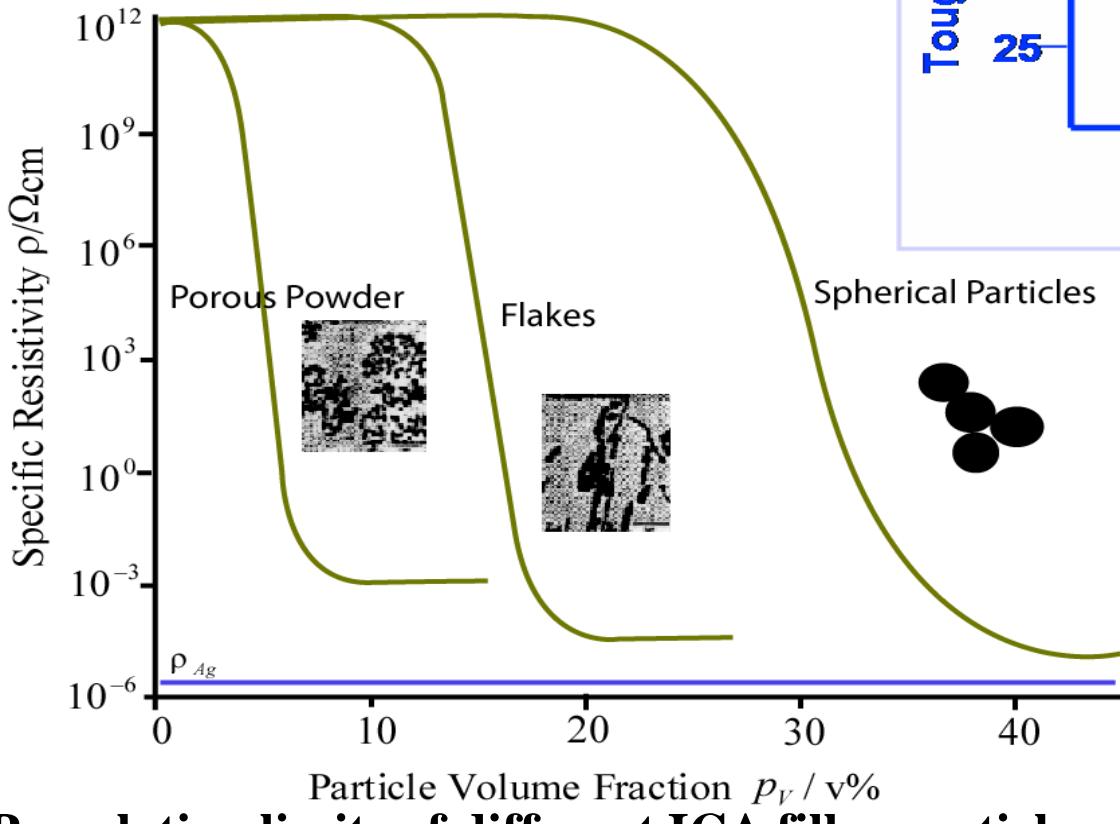
CTE/modulus reduction with less settling



- Polymer/metal composite example:
 Isotropic Conductive Adhesive (ICA)
- Percolation
- Polymer cure
- Electrical properties
- Reliability:
 - Drop test
 - Galvanic corrosion
- Miscellaneous
 - Magnetic alignment
 - Flip chip underfill filler
- Nanoparticles
- Carbon nanotubes (CNTs) & graphene

Nanoparticle Composites

(High surface/volume ratio
→catalysts, etc)



Nanoparticles → single grain, no defects
(Mallik) Incr surface area → incr adhesion

Added Ag more effective on conductivity as flakes or powder than as nanoparticles

Nanoparticle Sintering

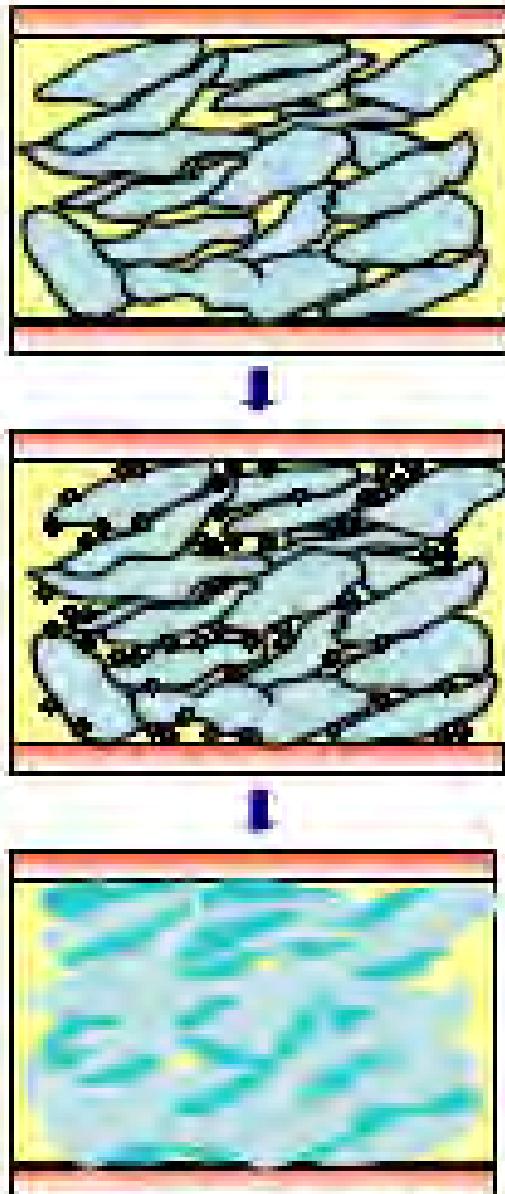
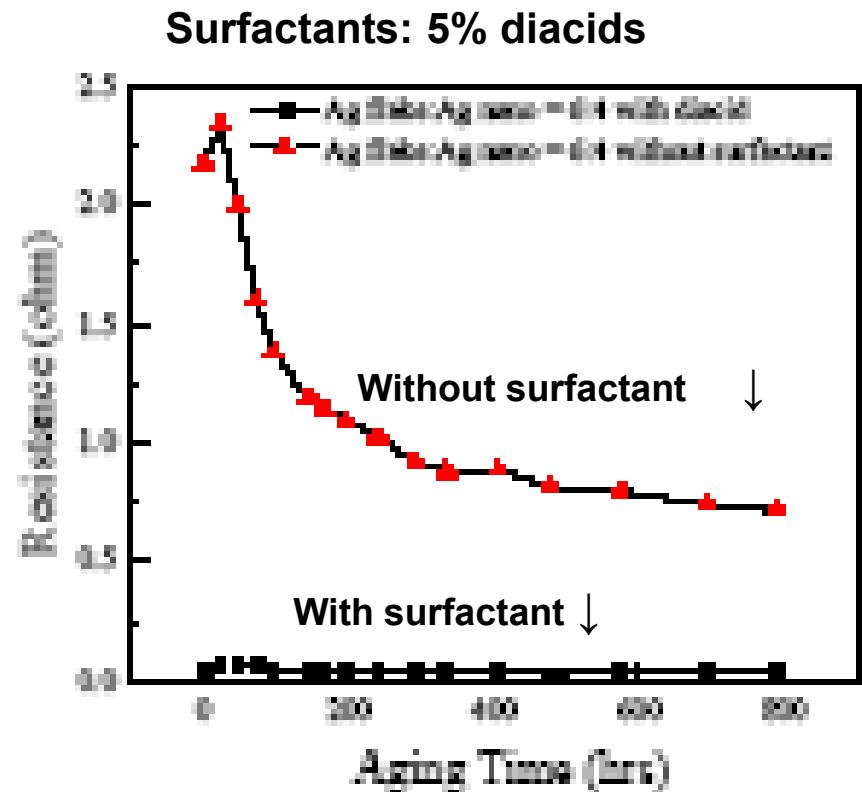


Figure 1. Schematic of particles and flakes between the metal and pads. (a) is conductive adhesives with silver flakes as fillers; (b) is conductive adhesives with both flakes and nanoparticles as fillers; (c) is conductive adhesives with sintered particles among flakes as fillers.



[Wong et al, ECTC '04 & '06]

Nanoparticle Sintering

- Sintering by surface self-diffusion, which is thermally activated, with net diffusion away from convex surfaces of high curvature.
- Particle interior retains crystallinity (not melting)

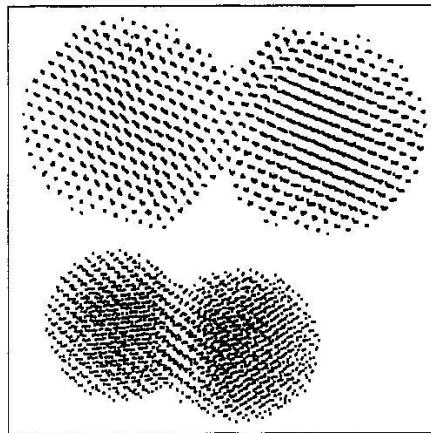


Figure 10. Side view of neck formation for particles of sizes 1014 and 2439 atoms.

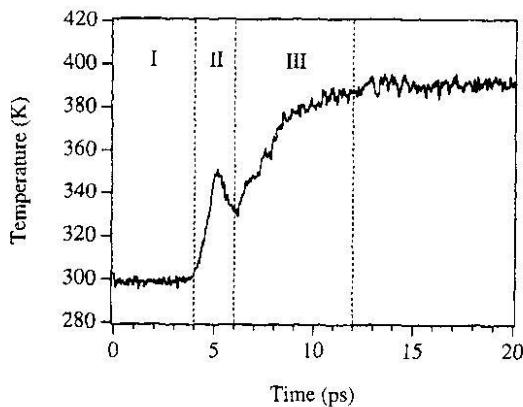


Figure 5. Variation of temperature of the system with time. This can be divided into three zones as explained in the text.

$$\frac{X^n}{R^m} = A(T) \cdot t \quad \text{where}$$

X = neck radius & R = sphere radius

Bulk diffusion : $n = 5$ $m = 2$

Surface diffusion : $n = 7$ $m = 3$

Surface diffusion dominates (Ohring)

$$t \propto (X / R)^7 R^4$$

Raut, Bhagat, Fichthorn,
Nanostruct. Mater. 10(5) 1998, 837-851

Embedded Components

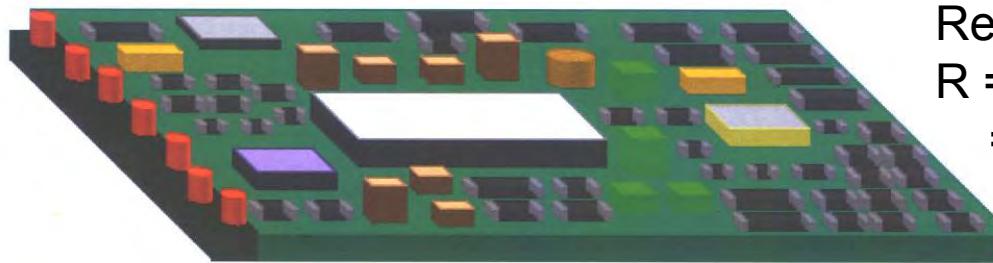


Figure 11: PWB vs SiP

Embedded capacitors:

C: Shrink area → shrink thickness for same C, i.e. μm scale → nm

Resistors (length L, width W, thickness t):
 $R = (L/W)(\rho/t)$
= Number of squares x resistance/square
Decrease t → increase R
decrease power

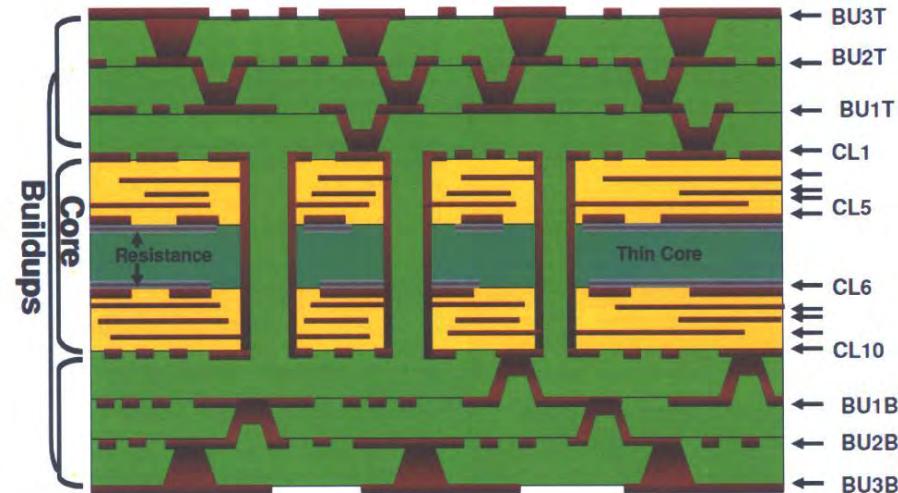


Figure 2: System in a Package (SiP): 3-10-3 cross section using resin coated copper capacitive (RC3) materials. Substrate cross section has resistance layers in the middle.

TCC control of nanocomposite capacitors:
High- k BaTiO_3 - & low- k BCB

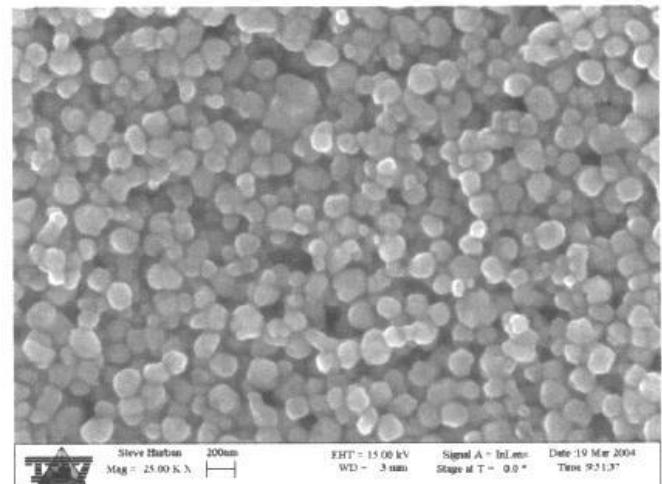


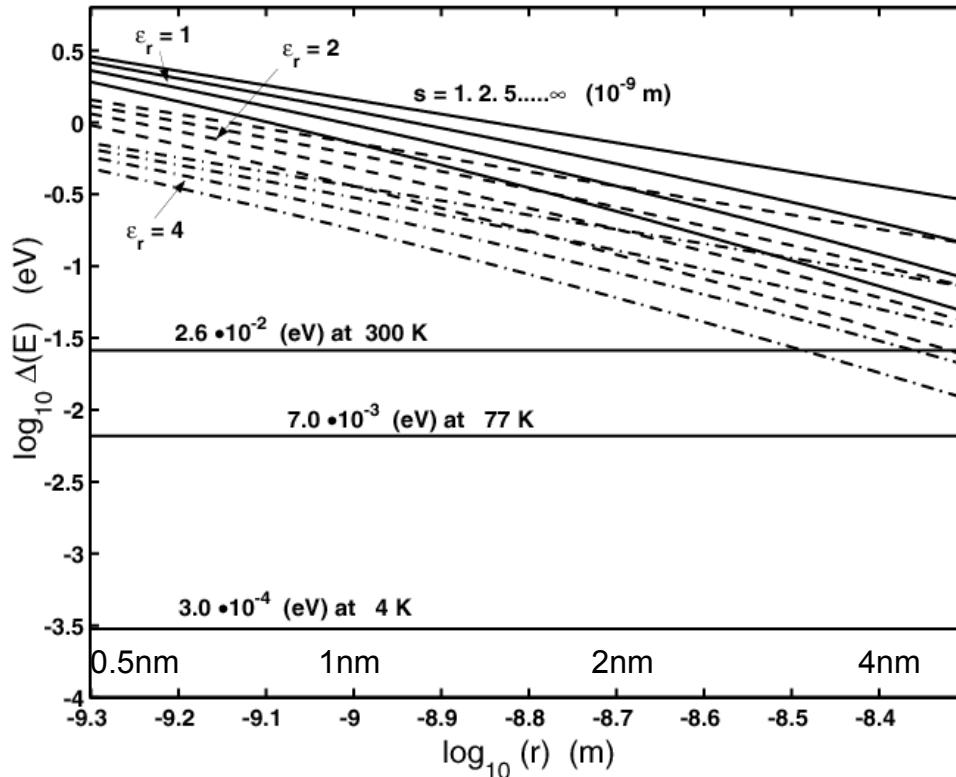
Figure 3: Larger area SEM images of RC3 nanocomposites.
[Abothu et al, ECTC'06]

Nanoparticle Charging:

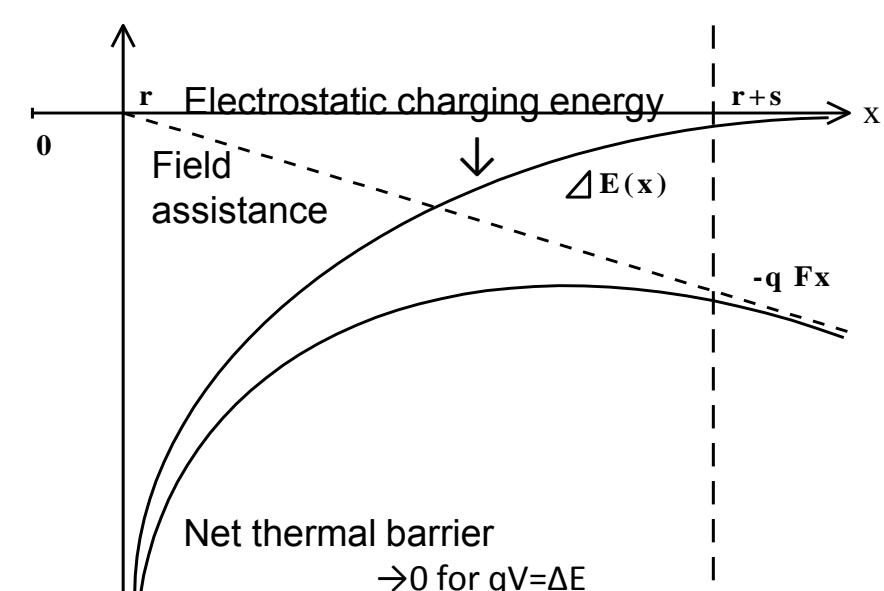
the Coulomb Block (Morris)

Spherical nanoparticles, radius r , separation s
Electrostatic charging energy:

$$\Delta E = \frac{q^2}{4\pi\epsilon r} \rightarrow \frac{q^2}{4\pi\epsilon} \left[\frac{1}{r} - \frac{1}{r+s} \right]$$



- The Coulomb blockade effect, which requires an external field or thermal source of electrostatic energy to charge an individual nanoparticle, and is the basis of single-electron transistor operation



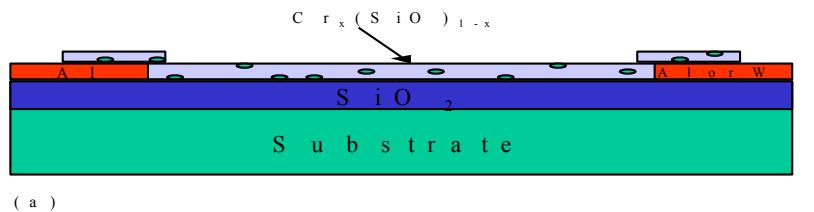
I-V characteristics of $\text{Cr}_x(\text{SiO})_{1-x}$



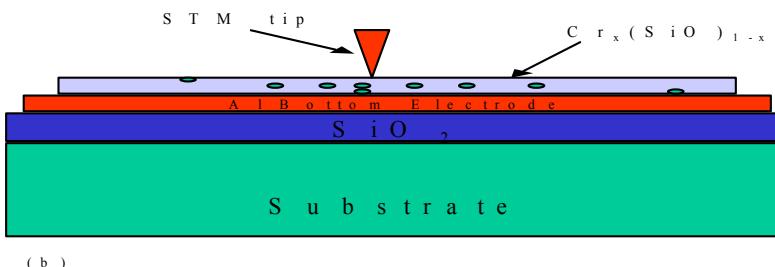
Portland State
UNIVERSITY

(Wu & Morris)

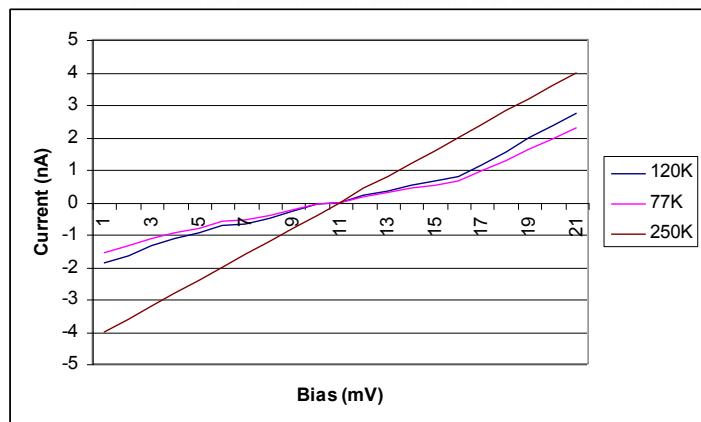
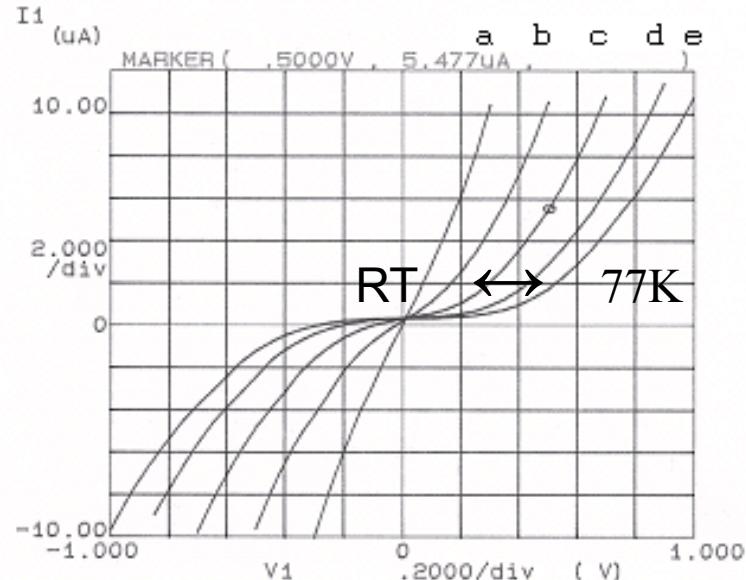
Electrical characteristics typical of Coulomb Blockade devices



(a)



(b)

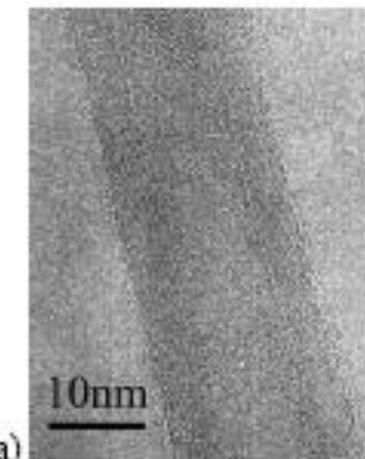
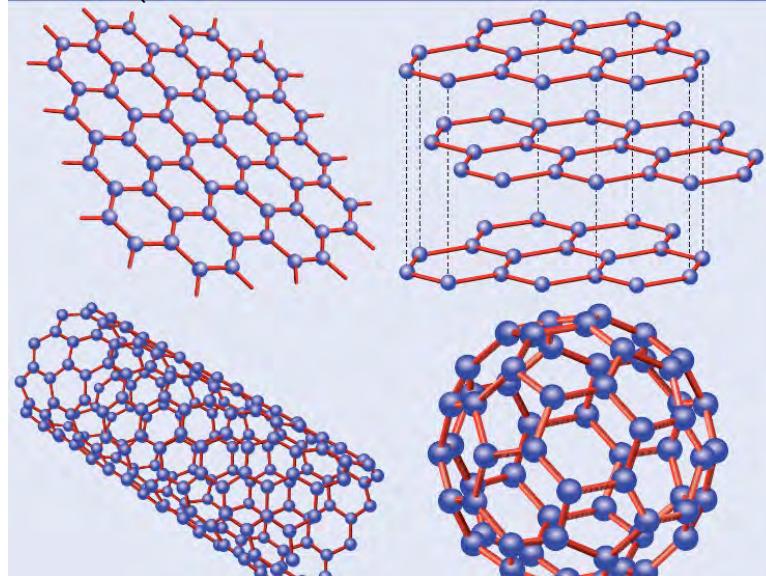


Coulomb effects “wash out” at room temperature (thermal charging) unless nanoparticles ~ single-nm scale

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 - Embedded components
- Carbon nanotubes (CNTs) & graphene
 - Electrical & thermal

Carbon Nanotubes (CNTs): SWNTs & MWNTs

(Kureshi & Hasan, J. Nanomaterials 2009, ID 486979)



Kyoung-Sik Moon et al,
ECTC'08

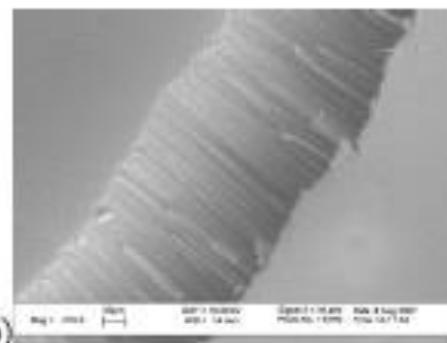


Figure 1. (a) TEM and (b) SEM images of aligned MWCNTs used.

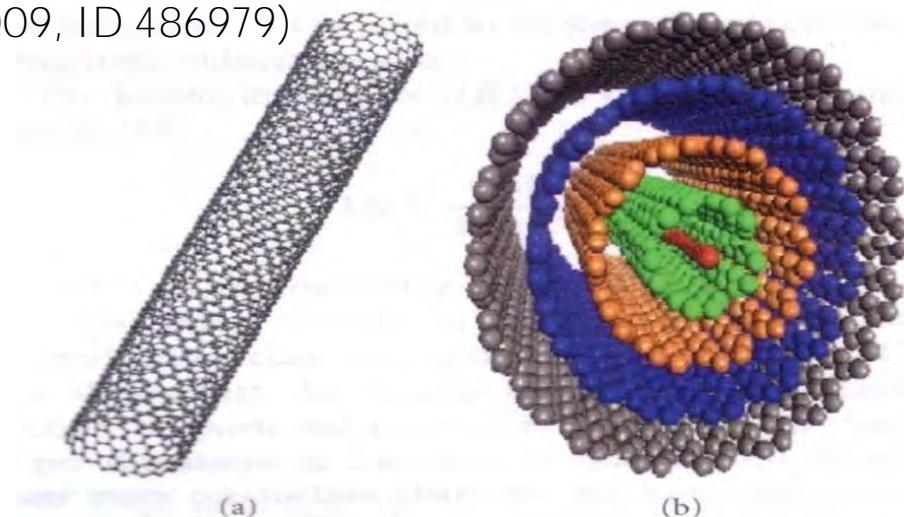
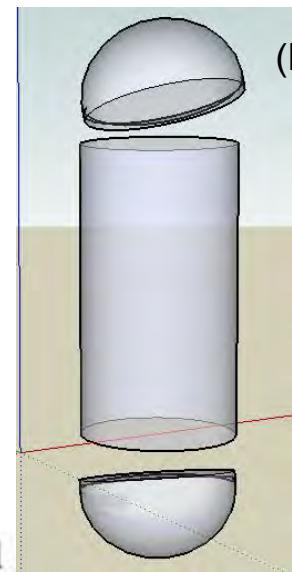


FIGURE 1: (a) Single-walled CNT. (b) Multi-walled CNT.



(Kunduru et al)

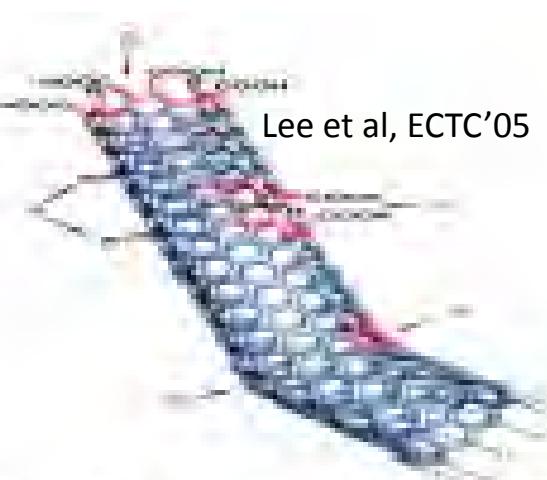
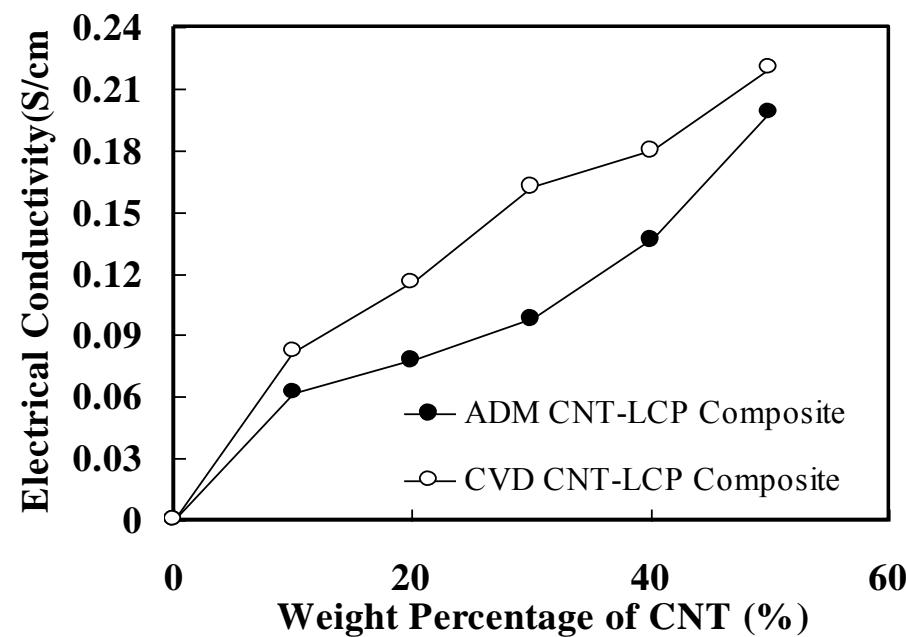
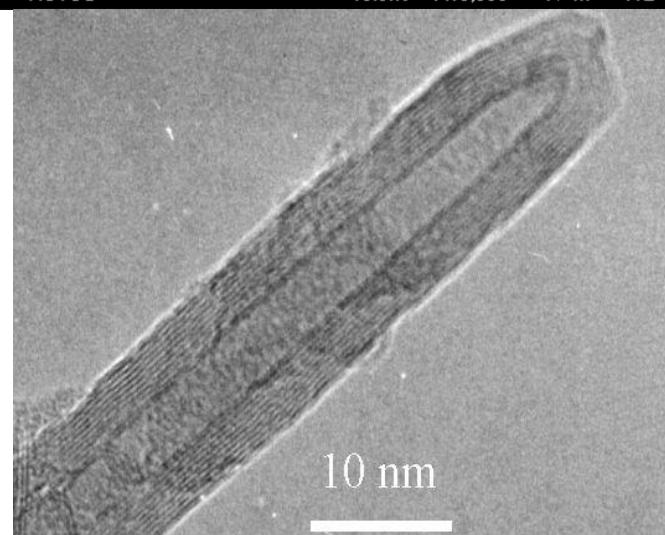
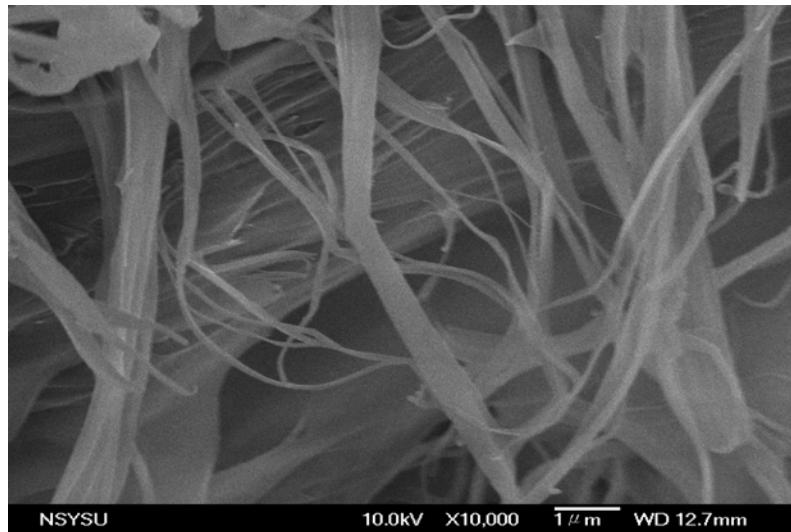


Figure 1. Acid-modified surface structure of CNT

EMC Shielding

MWCNTs (Cheng et al)

CNTs in LCP



Shielding Improvement (Ionic Liquid) at low CNT content

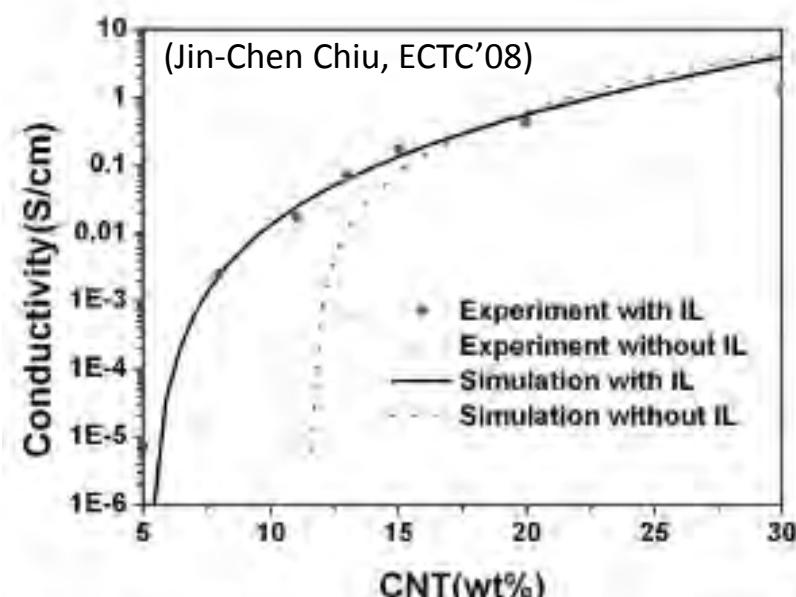


Figure 7 Conductivity of the MWCNT/PI composite at various weight percentage of MWCNT

CNT Composites Conductivity

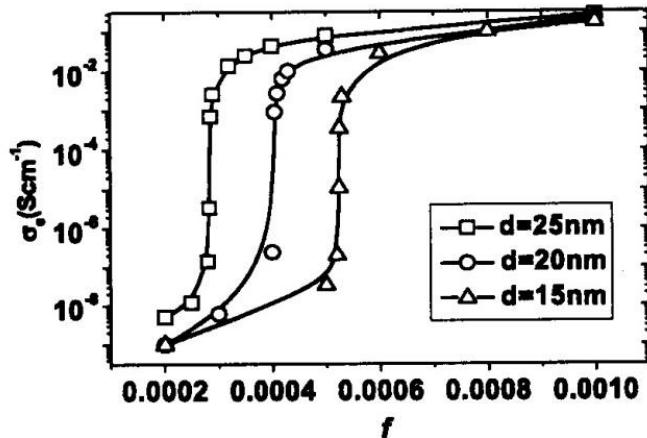


Figure 4. The dependence of the effective conductivities on CNT diameter d with different volume fraction f , with $\sigma_m = 10^{-9} \text{ S cm}^{-1}$, $\sigma_s = 1.85 \text{ S cm}^{-1}$, $\sigma_c = 1850 \text{ S cm}^{-1}$, $L = 2.5 \times 10^4 \text{ nm}$, $t = 2.5 \text{ nm}$.

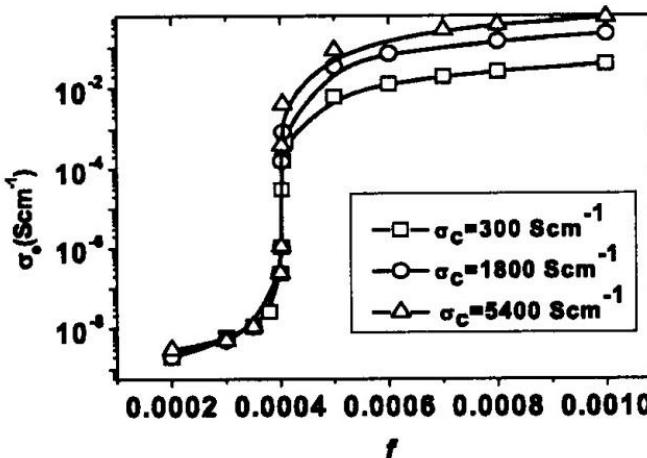


Figure 5. The dependence of the effective conductivities on CNT conductivity with different volume fractions f , with $\sigma_m = 10^{-9} \text{ S cm}^{-1}$, $\sigma_s = 1.85 \text{ S cm}^{-1}$, $L = 2.5 \times 10^4 \text{ nm}$, $d = 20 \text{ nm}$, $t = 2.5 \text{ nm}$.

Yan et al, Nanotechnology 2007

Oh et al, Nanotechnology, 19 (2008) 495602 (7pp)

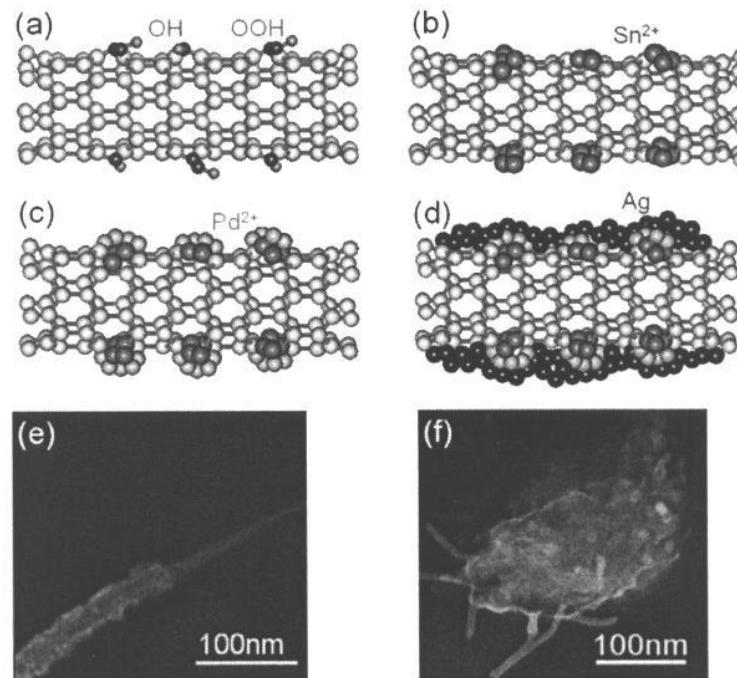
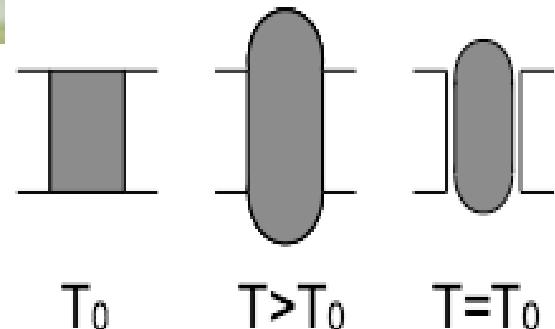


Figure 3. A schematic of electroless silver plating on carbon nanotubes: (a) carboxyl group functionalized nanotubes by the acid treatment process, (b) Sn^{2+} sensitization, (c) preactivation of nanotubes by Pd^{2+} , (d) electroless silver plating, (e) SEM image of the electroless-plated silver on a single MWNT, (f) a lump of silver sandwiching multiple MWNTs.

TSV reliability issues

(Sinha et al, NMDC 2010)

- a) Cu filled via at normal temperature
- b) Copper expansion can fracture the oxide layer above
- c) Delamination as a result of thermal cycling



(Metallic) SWNT thermal expansion coefficient

(Jiang et al, J. Eng Materials & Technology, 126 (2004) 265-270)

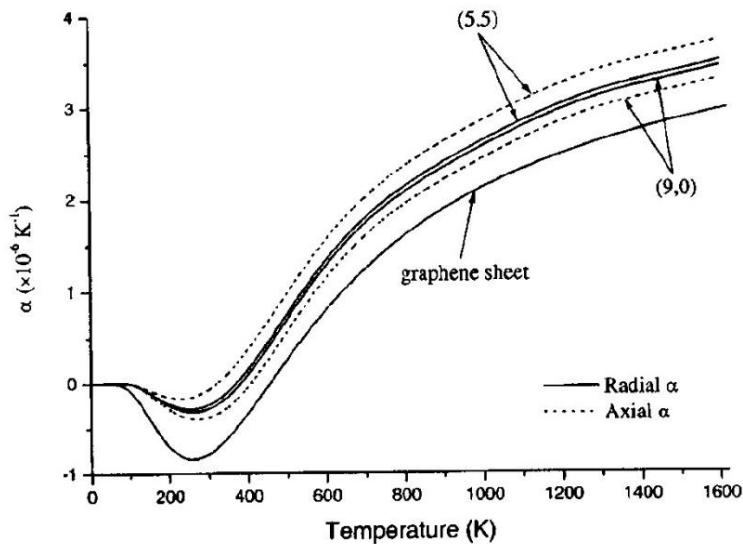


Fig. 2 The temperature dependence of the radial and axial coefficients of thermal expansion for (5,5) and (9,0) carbon nanotubes together with that for a flat graphene sheet

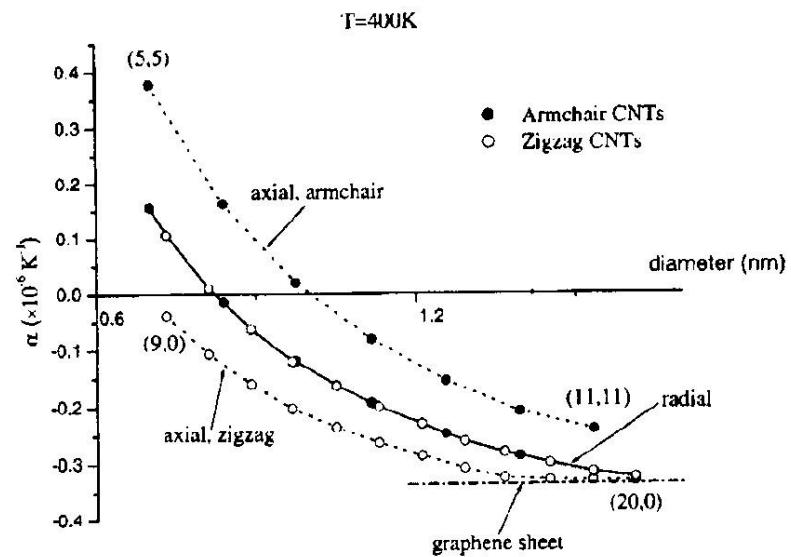


Fig. 4 The diameter-dependence of the coefficients of thermal expansion for armchair and zigzag carbon nanotubes at 400 K

Thermal Management in Microelectronics: Graphene & CNTs

Balandin, Advancing Microelectronics, 38(4) July/August 2011, 6-10

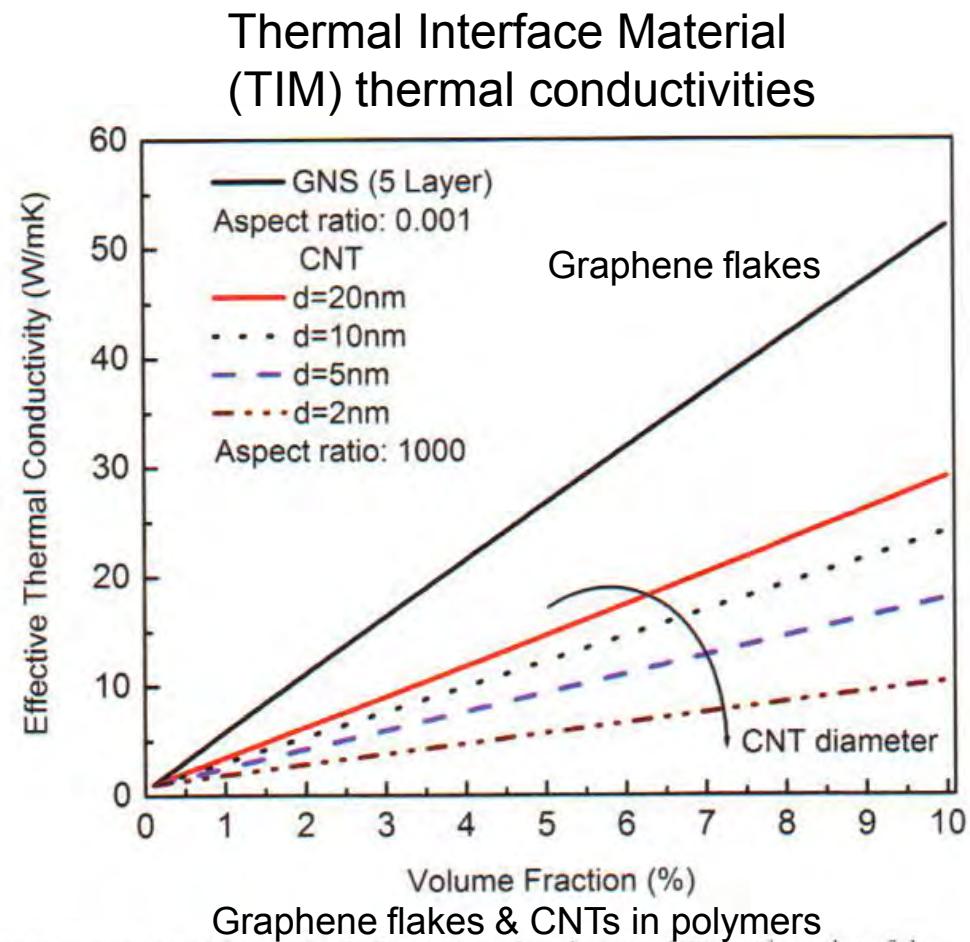
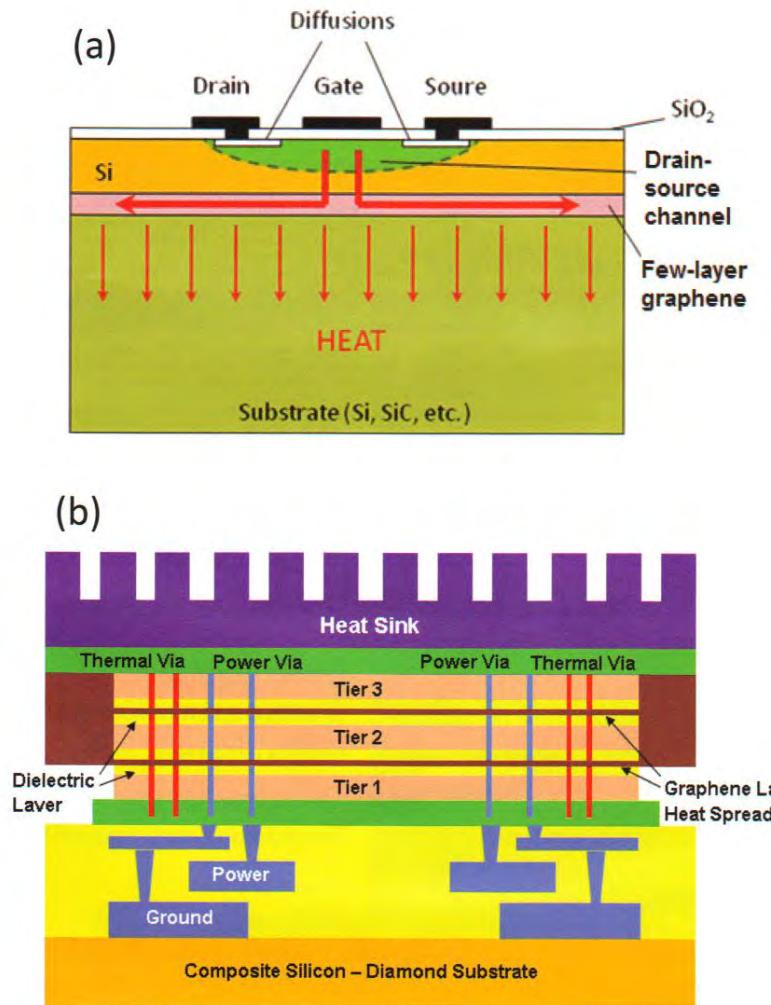


Figure 2: Comparison of the calculated effective thermal conductivity of TIMs with graphene flakes, marked as GNS, and CNTs. It is assumed that $K_p/K_b \sim 1000$, which is characteristic for typical carbon fillers and polymer matrix materials.

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Questions?